

# **Connectivity approach for flow and sediment delivery and application to SDR assessment**



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# This presentation have as subject the concept of **CONNECTIVITY** and their application in the context of soil erosion and conservation models: the *flow connectivity approach (FCA)*

*Hydrological connectivity is a term often used to describe the internal linkages between runoff and sediment sources in upper parts of catchments and the corresponding sinks (Croke et al., 2005).*



# Definition of connectivity for sediment flow:

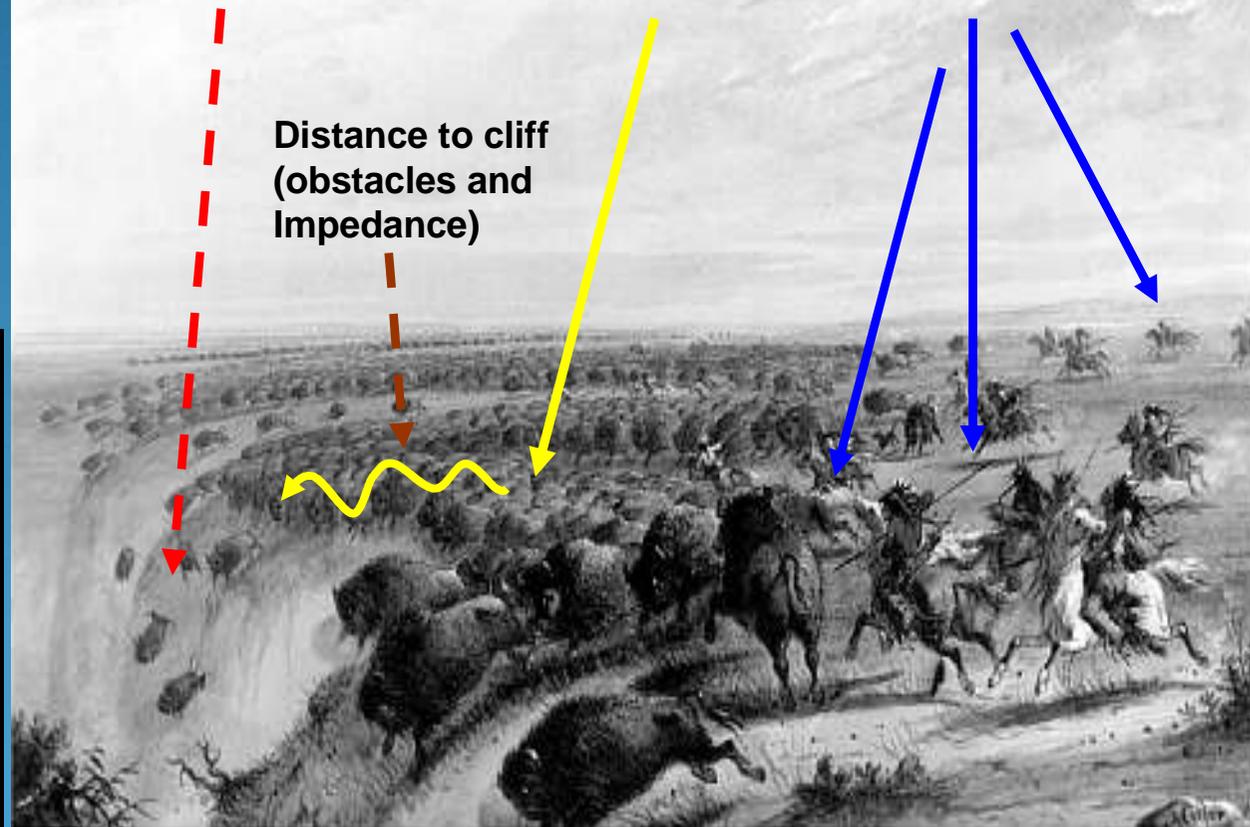
Connectivity is defined as chances that a particle has to reach the nearest sink  
It depends on: distance to the sink ; characteristics of the route ; water available to transport from upslope ; water that is gained/lost along the downslope route



The previous characteristics are defined and used, by many soil erosion distributed models in modelling and computation Of erosion end deposition In whole catchments

## A conceptual example of importance of connectivity

Buffalo Flow rate, Compression and storage, Driving force



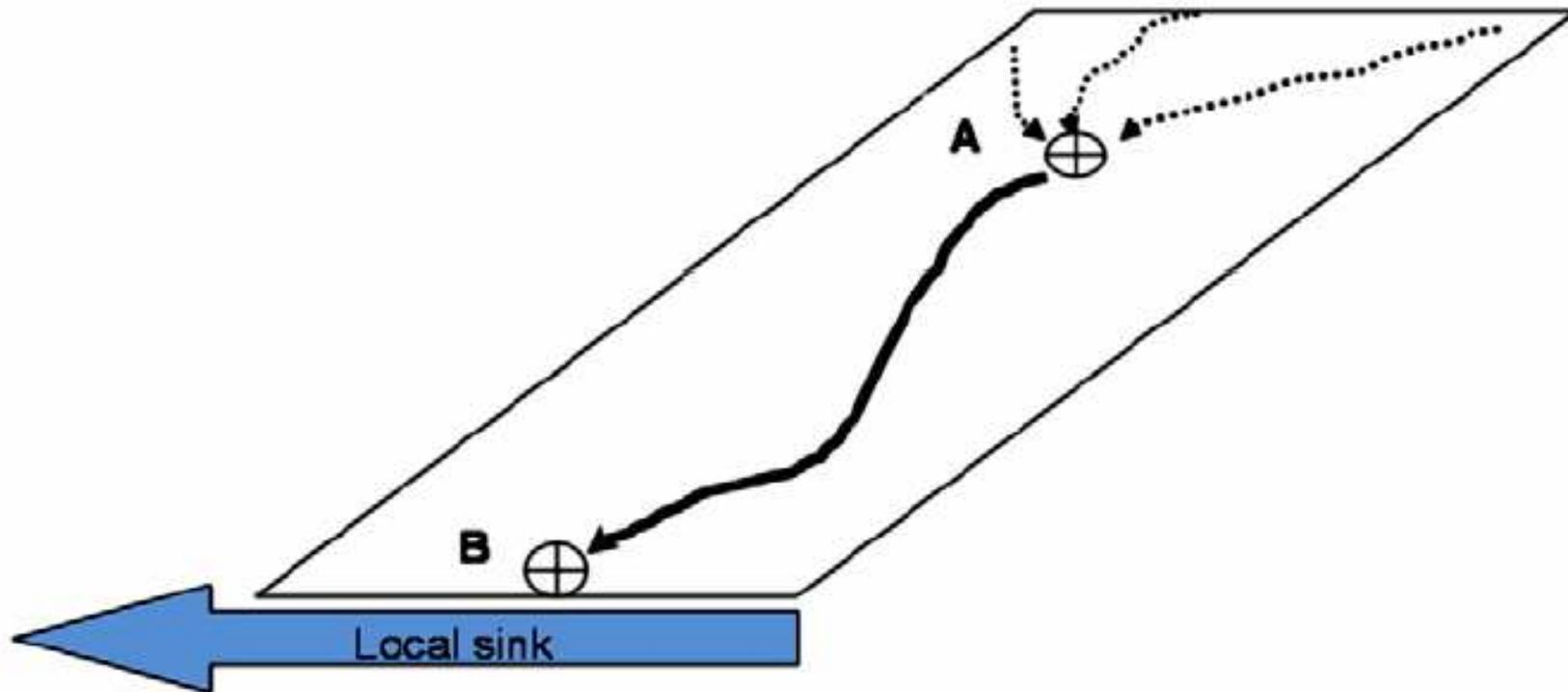
Distance to cliff (obstacles and Impedance)

*The **Buffalo jump**  
A Native Americans' Hunting technique  
That Have some similitude  
with soil erosion /runoff  
processes  
e.g. The chance of each  
buffalo to fall .... and die.*

Source: Alfred J. Miller 1887 from National Archives of Canada

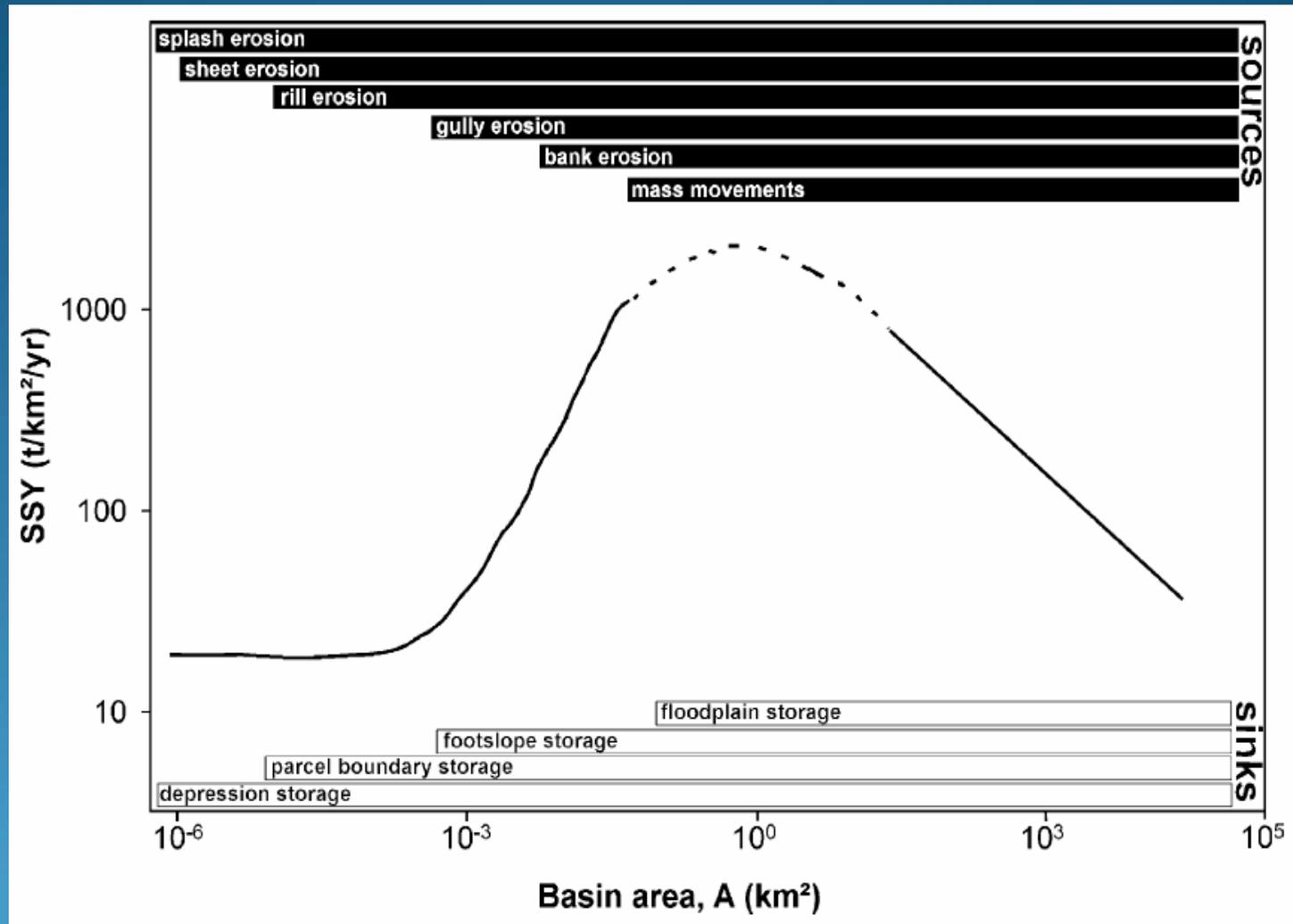
Diffuse connectivity Cammeraat (2002) it is influenced by:

- 1) soil surface irregularity (roughness), which could be very low on the patch scale, but higher at the hillslope and catchment scales,
- 2) spatial organization of the vegetation on the hillslope scale and the spatial arrangement between land units at the catchment scale,
- 3) rainfall intensity, event duration and thus the effective rainfall.



# ...Influence of Connectivity on sediment yield

SOURCES



SINKS

Conceptual model of sediment yield at various scale and contributing Sources and sinks (De Vente and Poesen (2005))

## ... Influence of Connectivity on sediment yield

*J. de Vente, J. Poesen / Earth-Science Reviews 71 (2005) 95–125*

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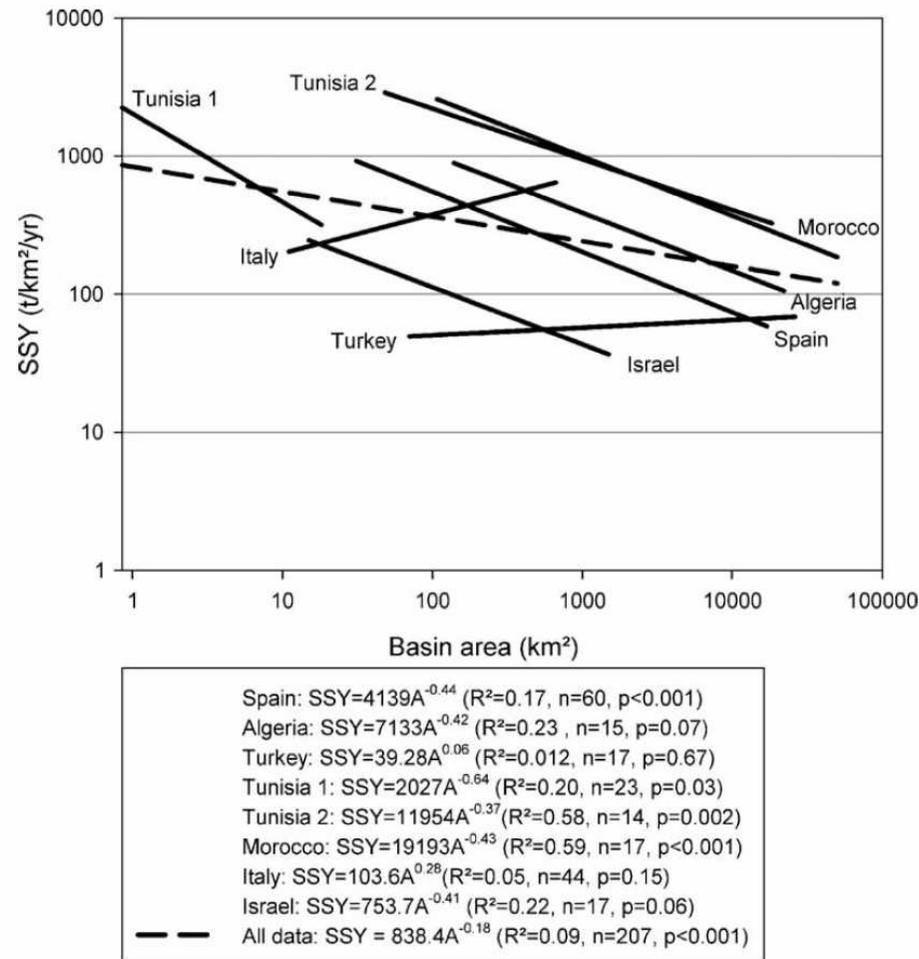


Fig. 3. Relation between area-specific sediment yield (SSY) and basin area for various Mediterranean basins. Source of data: Spain: (Avendaño Salas et al., 1997); Algeria: (Tidjani et al., 1998); Turkey: (Gögüs and Yener, 1997); Tunisia 1: (Albergel et al., 2000); Tunisia 2: (Lahlou, 1996); Morocco: (Lahlou, 1996; Fox et al., 1997); Italy: (Tamburino et al., 1990; Van Rompaey et al., 2003a; Van Rompaey et al., 2005); Israel: (Inbar, 1992).

## Sediment delivery at field and watershed scale

The prediction of sediment yield at basin scale is sometime done coupling a soil erosion model with mathematical function expressing the sediment transport efficiency of the hillslopes and the channel network

*(Kirkby and Morgan 1980; Walling 1983, Ferro and Porto 2000).*

At mean annual temporal scale, the sediment transport efficiency of the hillslopes and the channel network is usually represented by the spatially lumped concept of basin sediment delivery ratio (SDR) *(Walling 1983).*

## Sediment delivery ratio - Definition and link to flow connectivity

**SDR** is used to reduce Gross erosion:

$$SDR = SSY / A$$

Where: **SSY** is average annual sediment yield per unit area, and **A** is average annual erosion over the same area.

$$SDR = \frac{\text{Net erosion (SSY)}}{\text{Gross erosion (A)}} \quad \text{where SDR [0.0 - 1.0]}$$

At hillslope scale, and at **mean annual temporal scale** the sediment delivery ratio **SDR** appears to be an estimate of the efficiency with which materials eroded from hillslopes are delivered to the streams system (Boyce 1975).

Many factors influence SDR including hydrological inputs (mainly rainfall), landscape properties and complex interactions at the land surface (e.g. **vegetation, topography, and soil properties, roads, streams, ponds..**), so **CONNECTIVITY**.

## Role of flow connectivity Field observations



L. Borselli –Rutherglen (Victoria Australia)  
Department of Primary Industries (DPI) –  
September 25<sup>th</sup> 2009 –  
*Connectivity approach for flow and sediment  
delivery and application to SDR Assessment*

## Models for ASSESSMENT of SDR

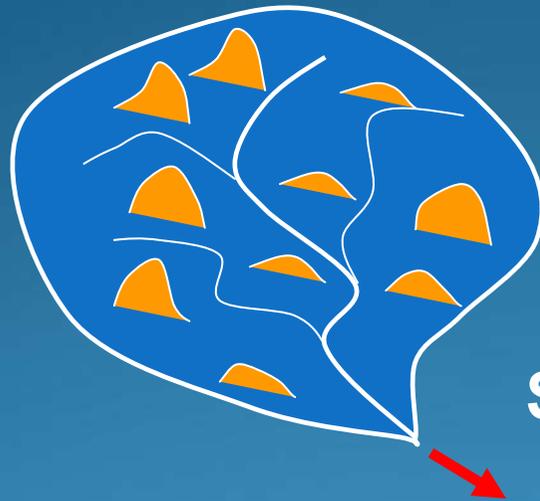
Various algorithms and methods exist for the assessment of sediment delivery ratio (SDR) at field or watershed scale :

- Geometrical topographical properties of watershed and drainage paths (Greenfield et al. 2001)
- Long term transport capacity assessment (Van Rompaey et al. 2001) - SEDEM
- Sediment properties and trap efficiency along the flow path (Lu et al. 2003).

Greenfield et al. (2001) , distinguish between 2 type of algorithms, both dominated by geometrical topographical properties of watershed and drainage paths:

- Drainage Area based models (UPSLOPE approach)
- Distance and slope models (DOWNSLOPE approach)

In case of **AREA BASED** models the SDR is applied to average erosion rate  $A$  computed for whole watersheds



*UPSLOPE approach*

$$SSY = A * SDR$$

In case of **DISTANCE/SLOPE BASED** models the SDR is applied to average erosion rate  $A_i$  computed for single pixels or morphological units



$$SSY_i = A_i * SDR_i$$

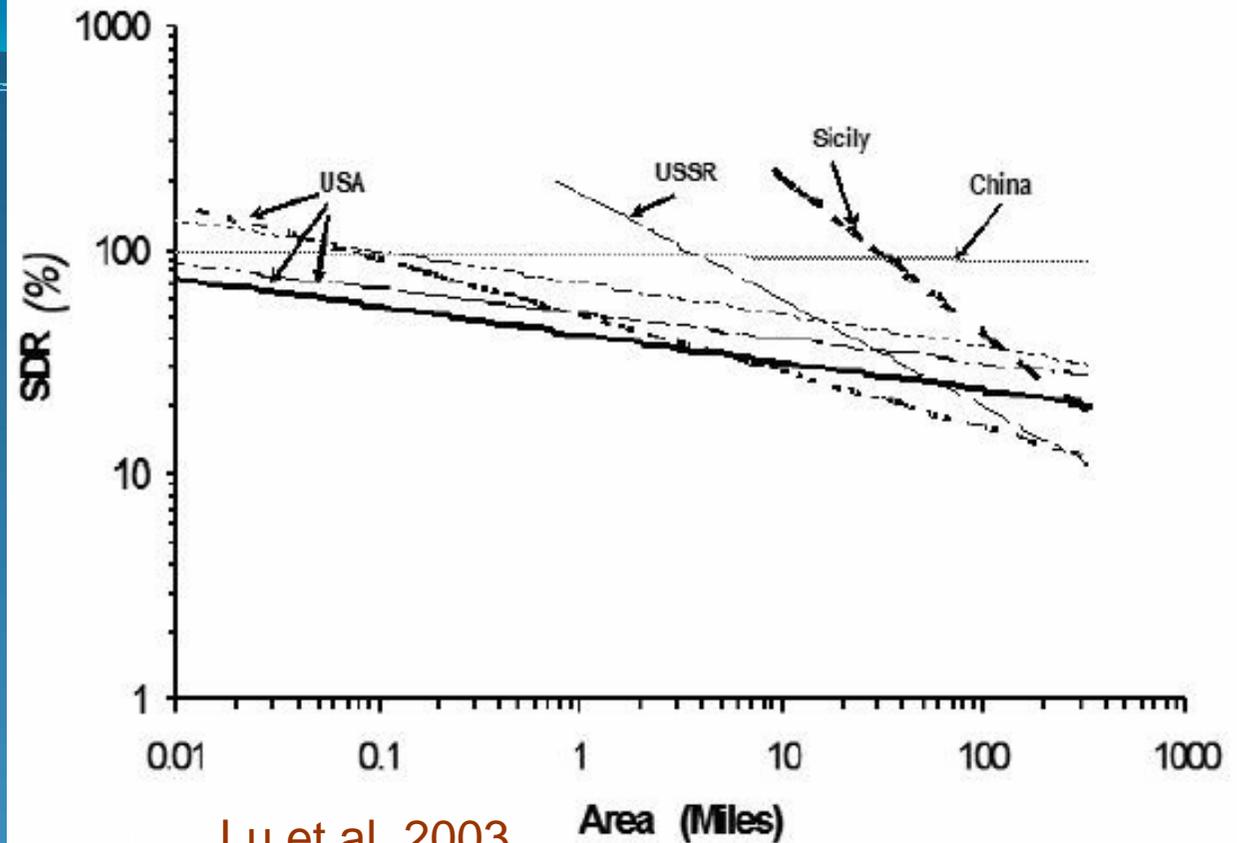
*DOWNSLOPE approach*  
-Spatial disaggregation-

## Drainage Area based models

$$SDR = \alpha A^{\beta}$$

$\beta \rightarrow [-0.7, -0.01]$

(Lu et al. 2003)



Lu et al. 2003

$$SDR = 0.418A^{-0.135} - 0.127$$

USDA-NRCS. 1983

***SDR* generally decreases with increasing basin size, because average slope decreases with increasing basin size, and large basins also have more sediment storage sites located between sediment source areas and the basin outlet, Boyce (1975)**

## Area based models

+ relief-length ratio and land use.. a variant

**Williams (1977)** found the sediment delivery ratio is correlated with drainage area, relief-length ratio, and runoff curve numbers. (Model based on the sediment yield data for 15 Texas basins).

$$\text{SDR} = 1.366 \times 10^{-11} (A)^{-0.0998} (ZL)^{0.3629} (CN)^{5.444}$$

Where:

A = the drainage area in km<sup>2</sup>,

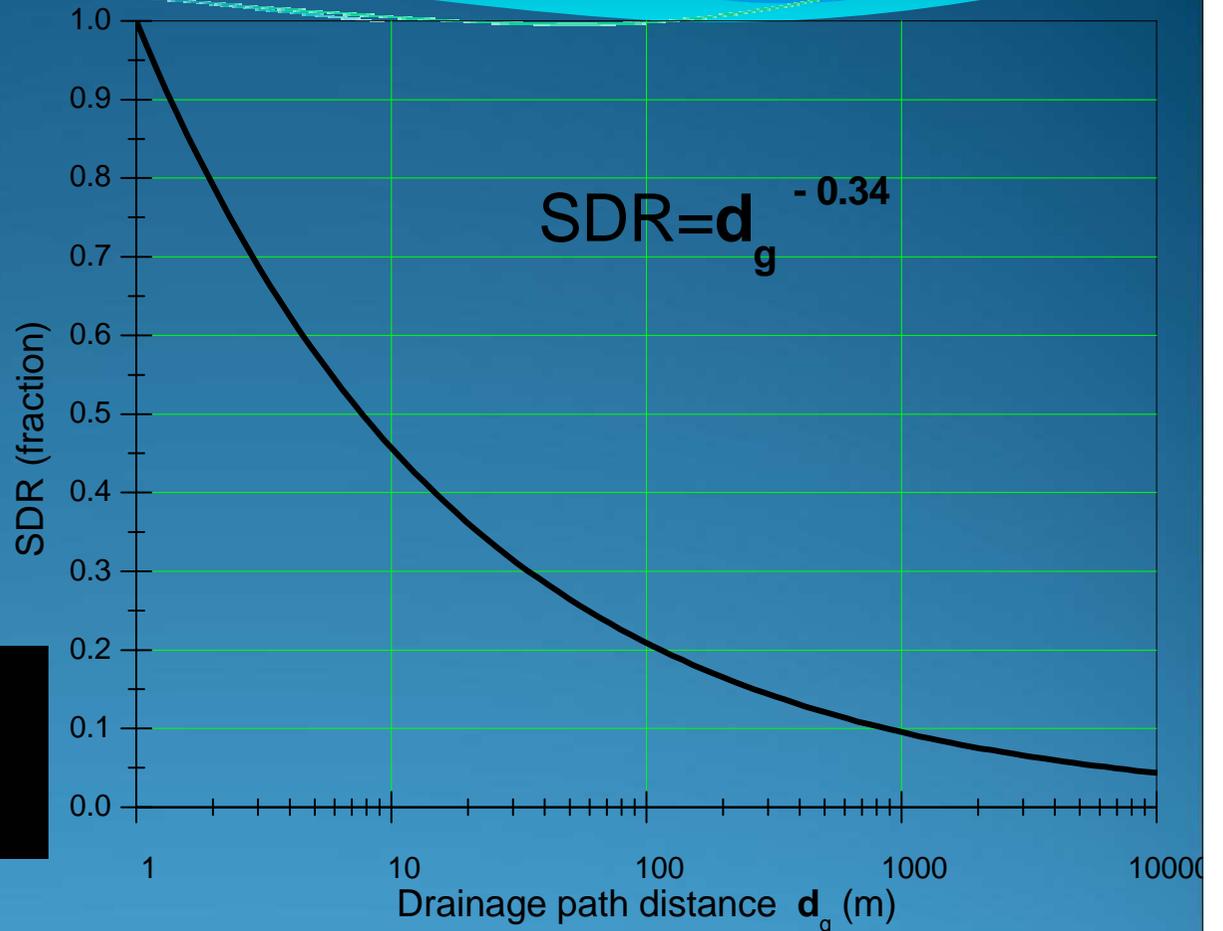
ZL = the relief-length ratio in m/km,

CN = the long-term average SCS curve number.

# Travel distance/slope models

from Novotny & Chesters (1981)

**Local slope gradient and length of path downslope to the nearest drainage line or sink.**



**(Sun and McNulty, 1998)**

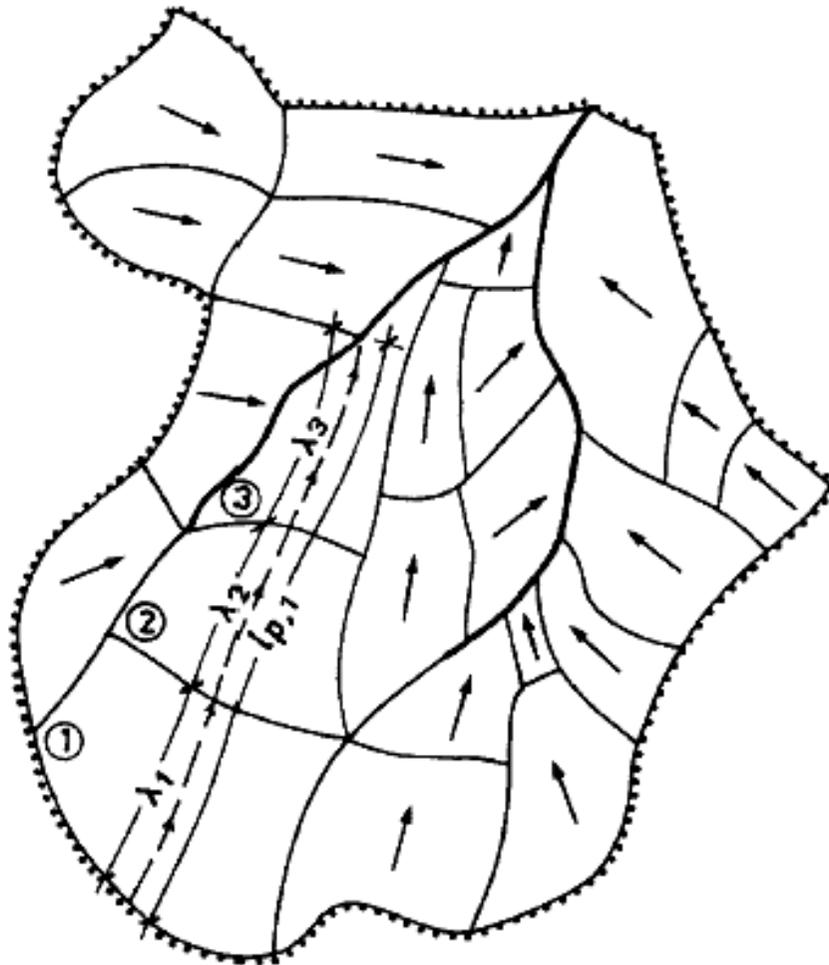
$$SDR = (1 - 0.97 * D/L)$$

$$\text{Where: } L = 5.1 * 1.79 * M$$

**Distance and slope-based equation (Yagow et al., 1988)**

$$SDR = \exp(-0.4233 * L * Sf)$$

$$\text{Where: } Sf = 0.6 + \exp(-16.1 * (r/L * 0.057))$$



- basin boundary
- stream
- morphological unit boundary
- main flow direction

FIG. 1. Scheme of Basin Discretized into Morphological U

## Ferro & Porto 2000 (SEDD model)

$$SDR_j = \exp \left[ -\beta \left( \sum_{j=1}^n \frac{\lambda_j}{\sqrt{s_j}} \right) \right]$$

$\beta$  = lumped calibration parameter  
 $\lambda$  = length along flow path  
 $s$  = slope along flow path

In this case SDR it is computed and applied at each morphological units to obtain the single sediment yield contribution

## How to relate flow connectivity and SDR

Remember the previous definition...

*The chances that a particle has to reach the nearest sink depends on: the distance to the sink, the characteristics of the route, the water available to transport from upslope, the water that is gained/lost along the downslope route.*

So the properties of the path to the nearest sink and the properties of the upslope contributing areas should be **CONCURRENT** to establish the potential connectivity.



## Local sinks at field scale

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# INDEX OF CONNECTIVITY (IC)

Hillslope sediment delivery processes and channel processes should be **considered** and modeled **separately** (Atkinson 1995).

We **concentrate** on **HILLSLOPE DOMAIN** and in our schematization we have defined the permanent drainage lines (streams), roads, urban areas, and lakes as **total sink**.

Land use and slope gradients along the downslope route, and path length, are used to rate the sinking potential. (***first component***)

Upslope catchment's areas, mean upslope and land use are used to rate the potential for down-routing. (***second component***)

Finally the **TWO COMPONENTS** are then used for defining an **INDEX OF CONNECTIVITY** (Ic).

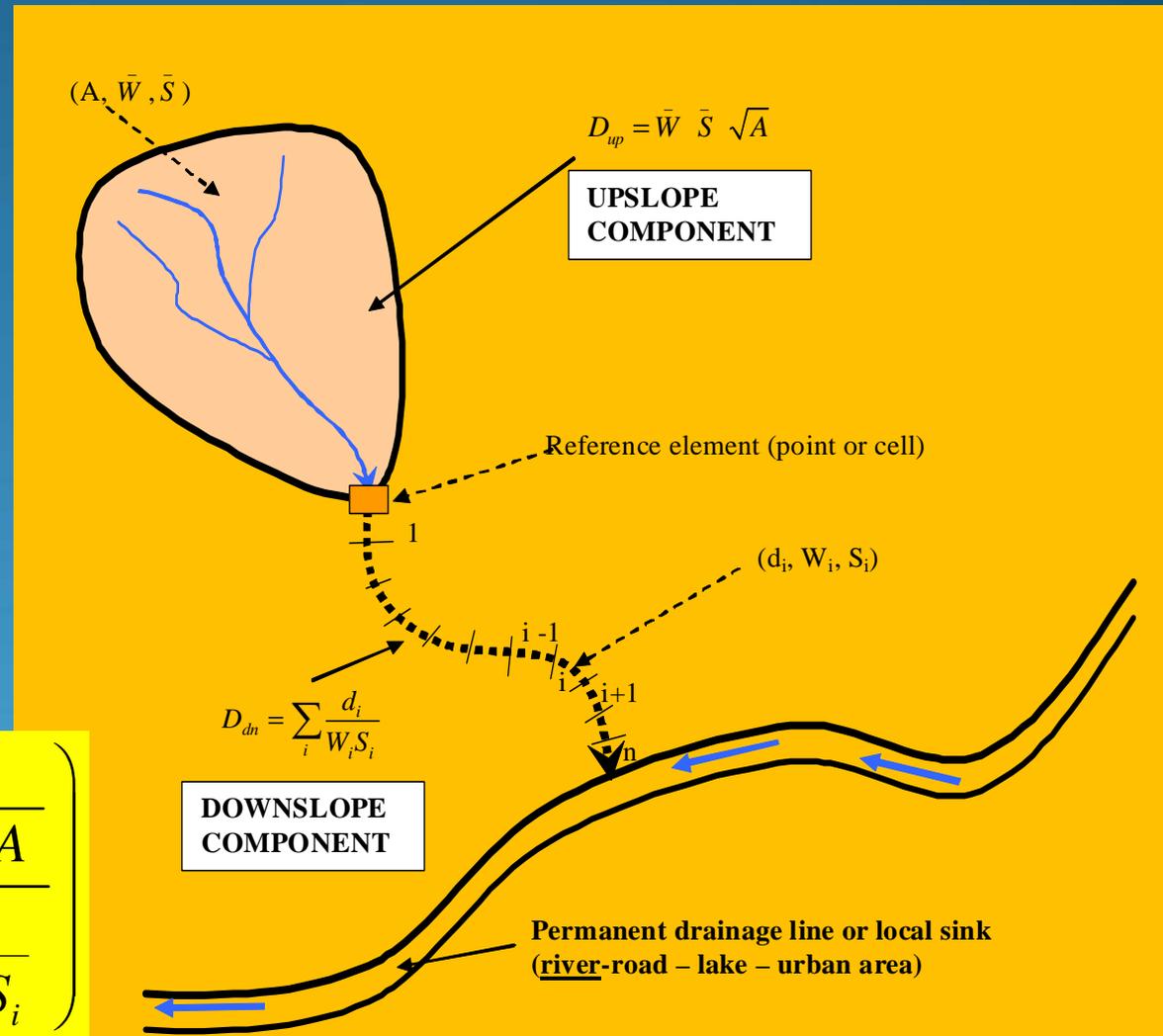
**best application with a spatial disaggregation defined by a 5X5 m resolution raster GIS**

# Connectivity index model – IC

Borselli et al. (2008). Prolegomena to Sediment and flows connectivity in the landscape: a GIS and field numerical assessment . CATENA(elsevier)

*The Connectivity Index (IC) value is computed using two components:*

- **Downslope component:** is the sinking potential due to the path length, land use and slope along the downslope route.
- **Upslope component:** is the potential for down routing due to upslope catchment's areas, mean upslope and land use.



$$IC = \log_{10} \left( \frac{D_{up}}{D_{dn}} \right) = \log_{10} \left( \frac{\bar{W} \bar{S} \sqrt{A}}{\sum_i \frac{d_i}{W_i S_i}} \right)$$

$$D_{dn} = \sum_i \frac{d_i}{W_i S_i}$$

## DOWNSLOPE Component

$d_i$  = length of cell  $i$  along the downslope path (in m)

$W_i$  = Weighting factor of cell  $i$  along the downslope path (adimensional)

$S_i$  = slope gradient of cell  $i$  along the downslope path (m/m)

$$D_{up} = \bar{W} \bar{S} \sqrt{A}$$

## UPSLOPE Component

$\bar{W}$  = average Weigthing factor of the upslope contributing area (adimensional);

$\bar{S}$  = average slope gradient of the upslope contributing area (m/m)

$A$  = upslope contributing area (m<sup>2</sup>)

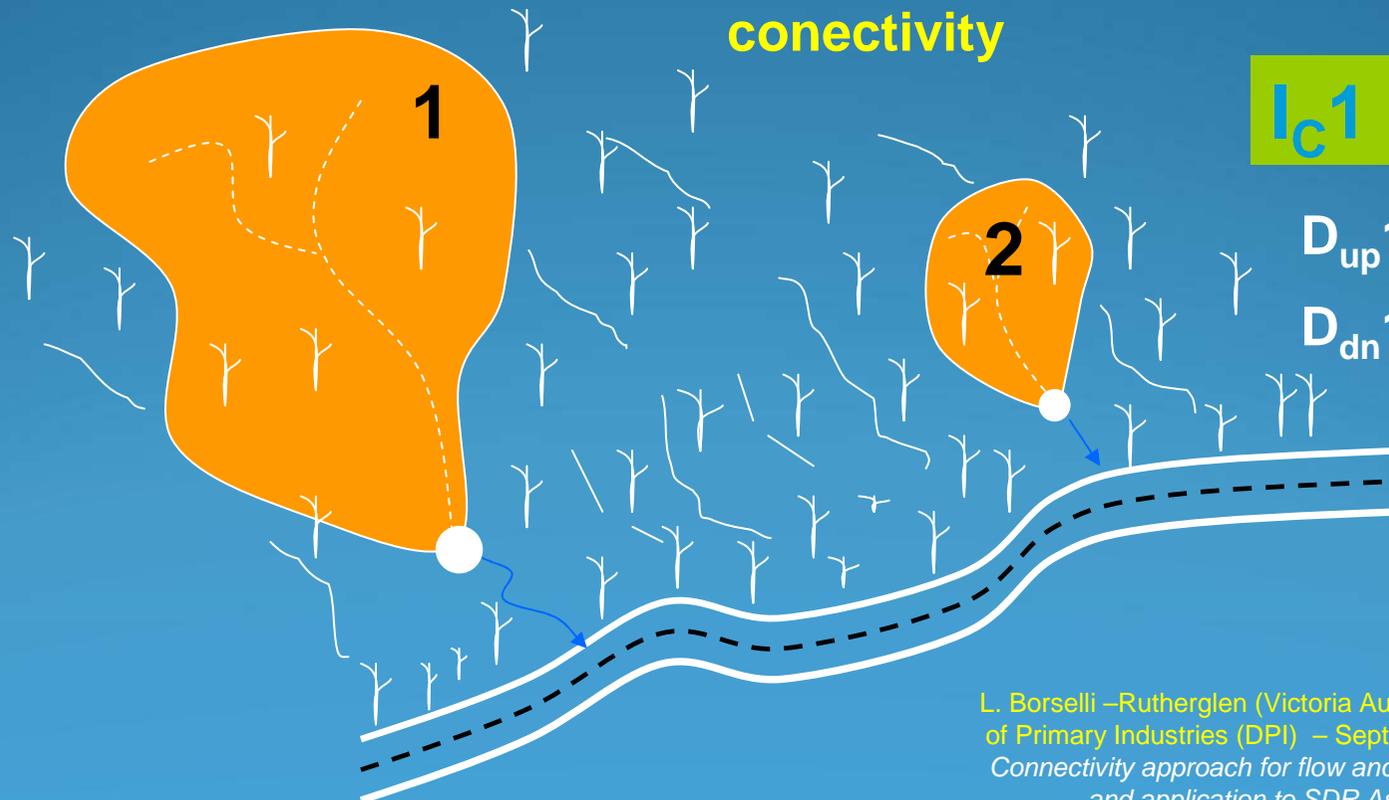
## Connectivity index ( $I_c$ )

$$IC = \log_{10} \left( \frac{D_{up}}{D_{dn}} \right) = \log_{10} \left( \frac{\bar{W} \bar{S} \sqrt{A}}{\sum_i \frac{d_i}{W_i S_i}} \right)$$

$I_c$  range:  $[-\infty, +\infty]$

Under this definition the local level of connectivity to permanent drainage lines/sinks is inversely proportional to  $I_c$ :

Values  $I_c > 0$  **high connectivity**  
Values  $I_c < 0$  **medium to low connectivity**



$$I_{c1} = I_{c2}$$

$$D_{up1} > D_{up2}$$

$$D_{dn1} < D_{dn2}$$

## Application of connectivity approach.

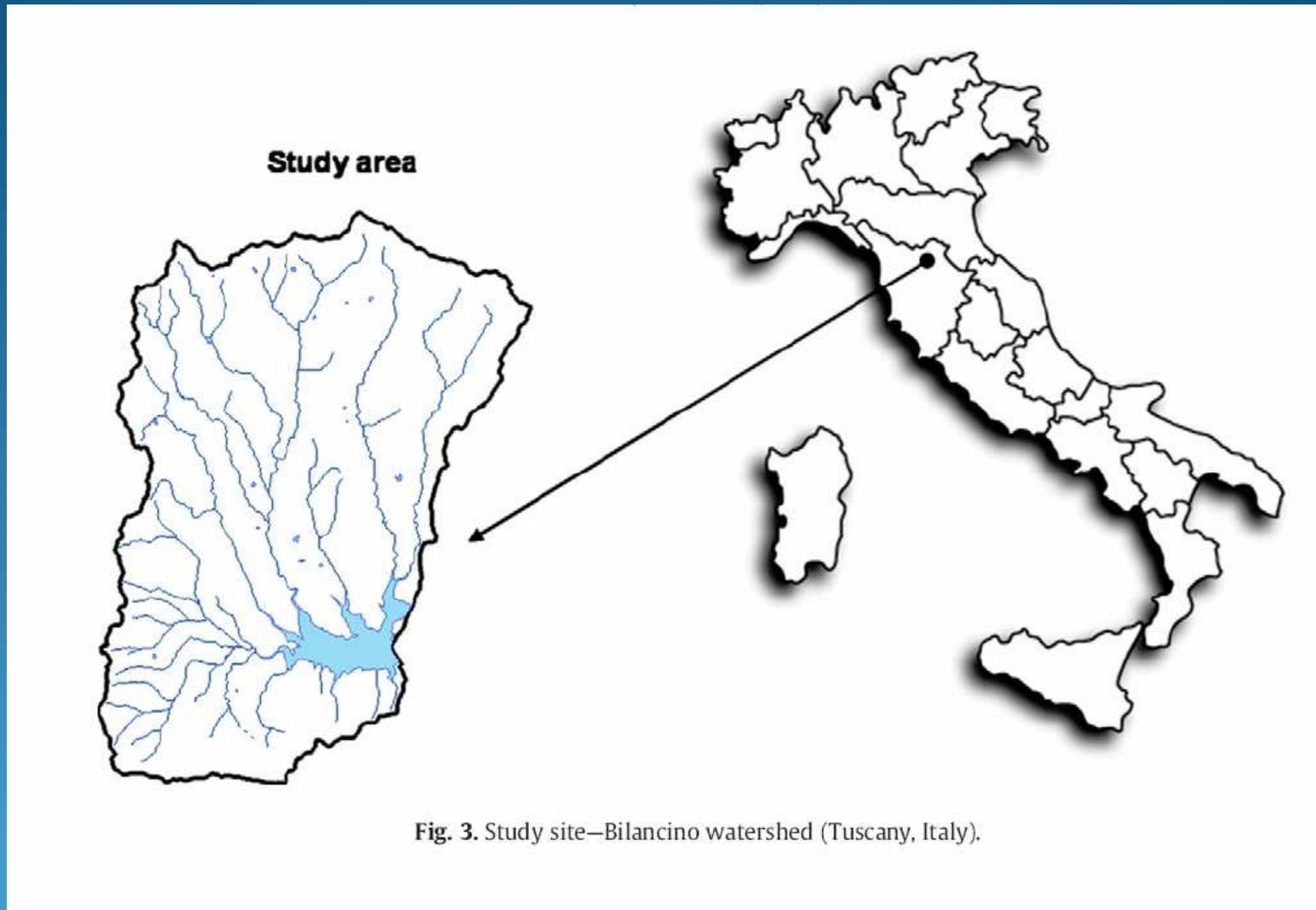
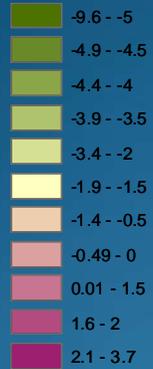
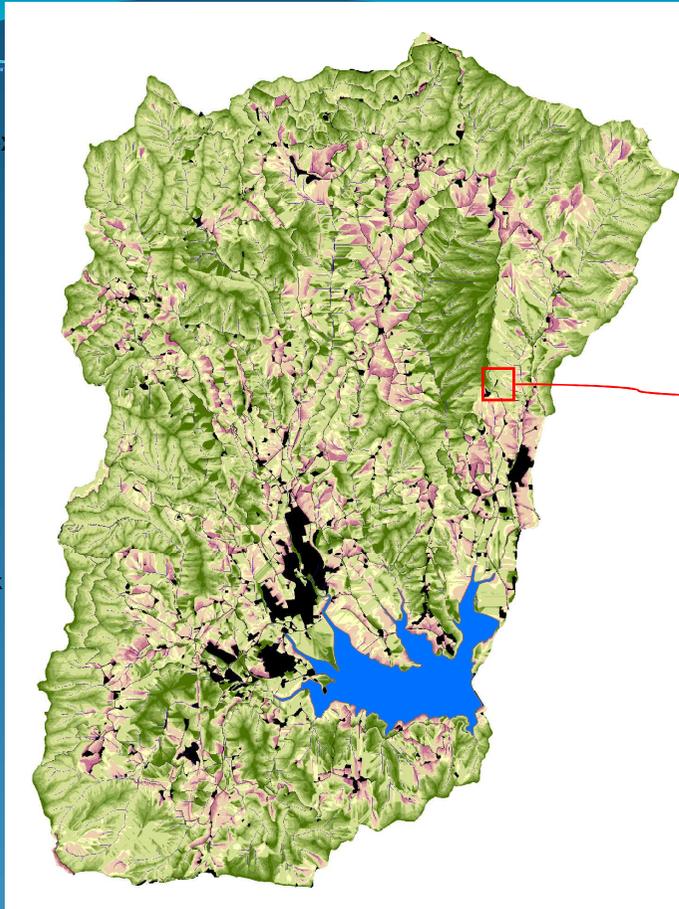


Fig. 3. Study site—Bilancino watershed (Tuscany, Italy).

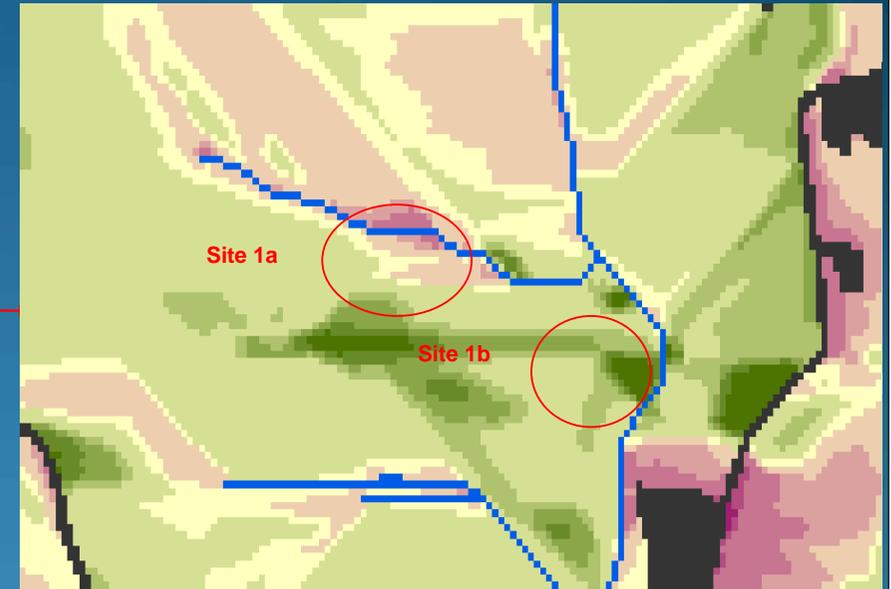
Connectivity fluxes index



In black the road/urban mask



IC map of deposition and connection areas evidenced in red



Site1a -Area in proximity of local sink at field bottom: direct connection of rill system without appreciable sedimentation



Site1b-Area in proximity of local sink at field bottom: direct connection of rill system relevant sedimentation

Application at watershed scale  
(Bilancino-Tuscany-Italy)-  
hot spot identification of primary  
sediment sources area.  
(Borselli et al. 2008)

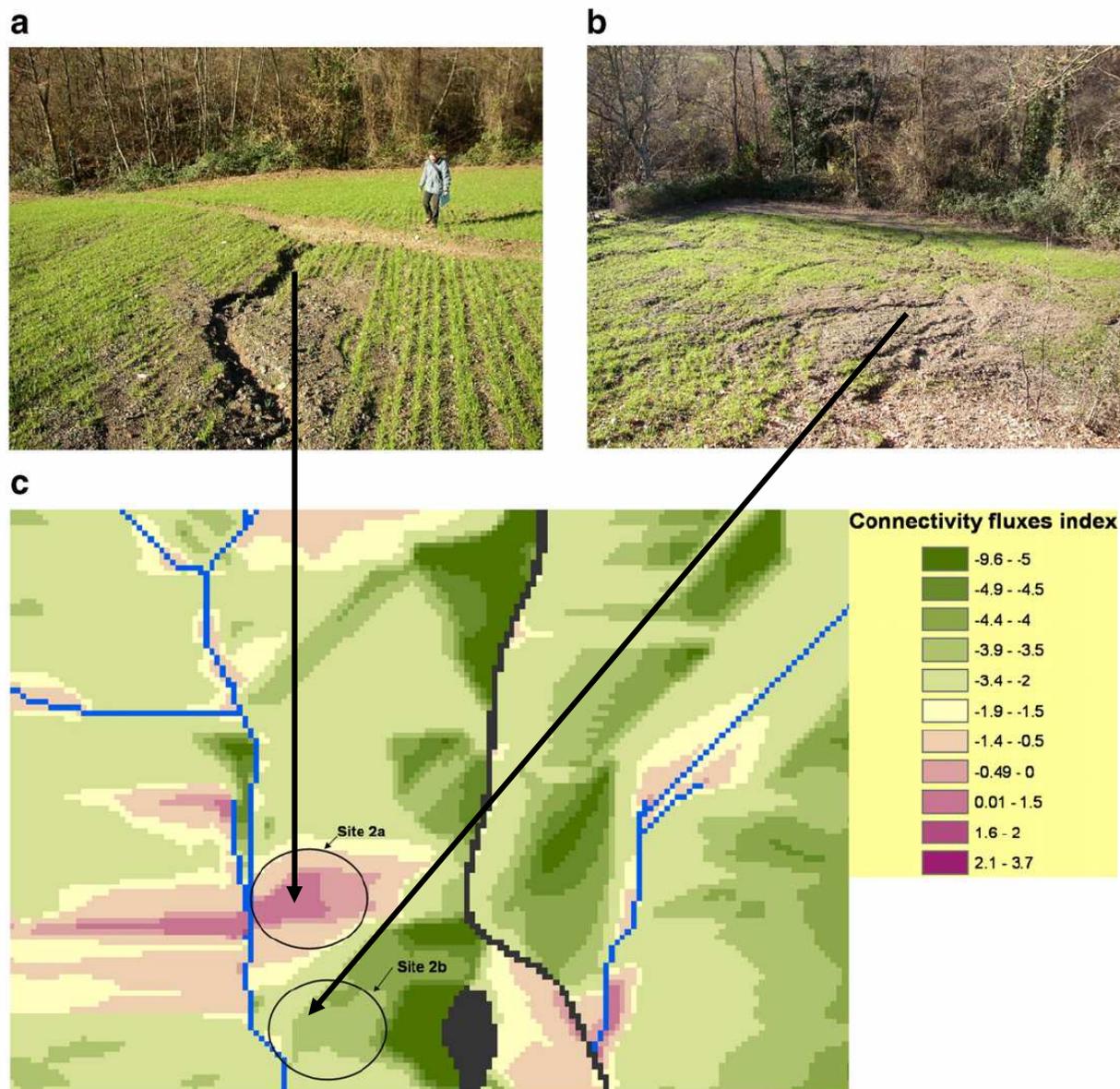


Fig. 1. Site 2—Area close to a local sink at the bottom of a field: direct connection of rill system without detectable sedimentation. b: Site 2—Area in proximity of local sink at the bottom of a field: direct connection of rill system with intense sedimentation. c: IC map of Site 2: deposition and connection areas are evidenced inside circular areas.

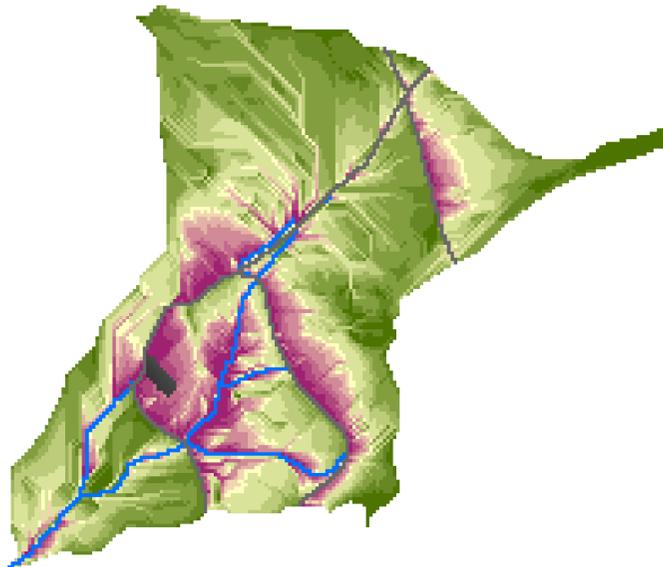
# Scenario analysis of connenctivity evolution due to land management practice

Prevailing land use of the watershed is wheat crop. The connectivity index is evaluated before and after harvesting (June) when the borders of the fields are ploughed for 5 meters wide.



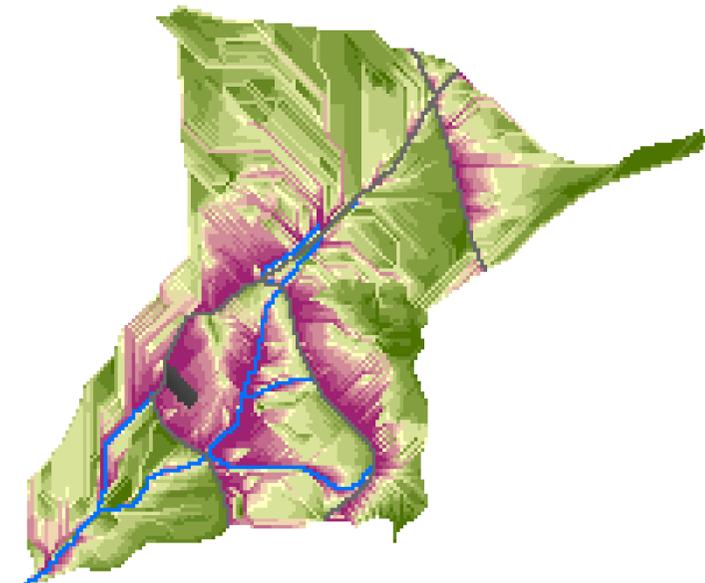
Without strip of bared soil on field border

With strip of bared soil on field border

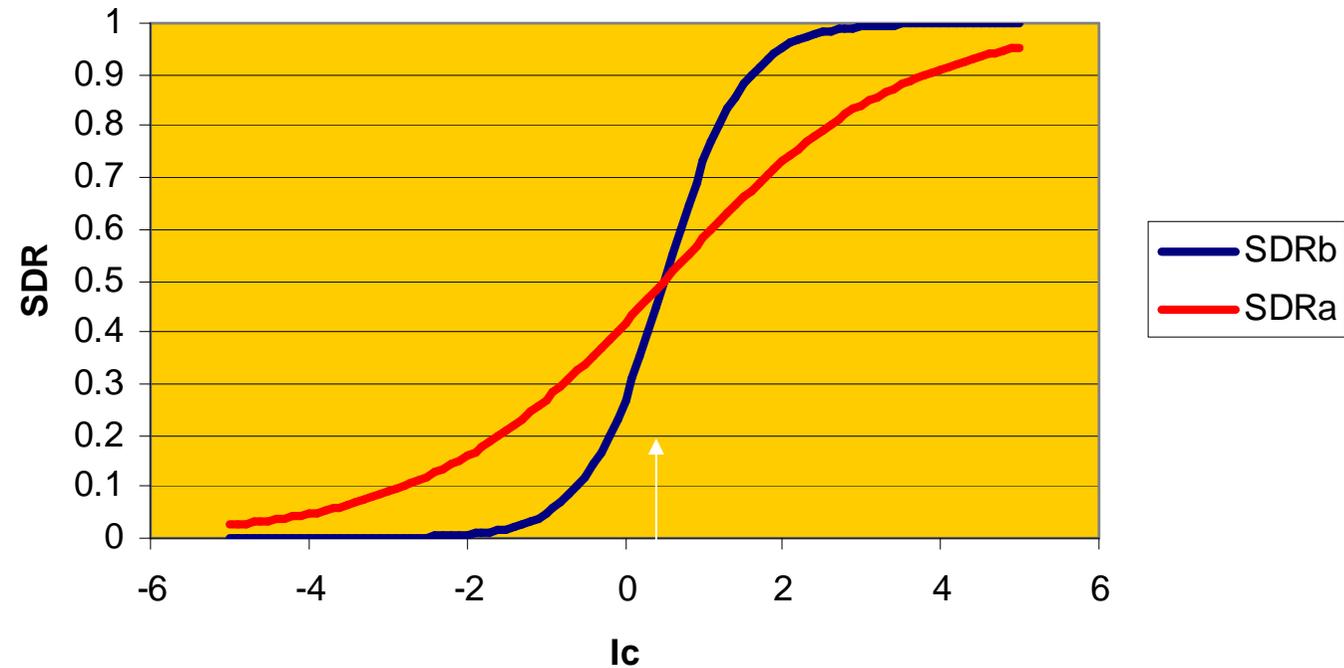


### Connectivity fluxes index

- 4.1 - -2
- 1.9 - -1.5
- 1.4 - -1
- 0.9 - -0.8
- 0.79 - -0.5
- 0.49 - -0.1
- 0.09 - 0
- 0.01 - 0.1
- 0.11 - 0.25
- 0.26 - 0.5
- 0.51 - 0.66
- 0.67 - 1
- 1.1 - 1.5



Possible functional relationships between  $I_c$  and SDR...



*Boltzmann type function ..  $SDR=f(IC, IC_0, k)$   
(Borselli et al. 2007)*

$$SDR = \frac{1}{1 + \exp\left(\frac{IC_0 - IC}{k}\right)}$$

## FIC – THE FIELD APPROACH

The field assessment of connectivity is evaluated using the same approach of  $I_c$ , i.e. estimating the upslope and the downslope component. A well defined field connectivity index ( $FIC$ ) can permit an evaluation of the GIS-based  $IC$ . As  $FIC$  is strictly related with the event that produced the connectivity evidence, it is also a way of representing ground truth. Hence a comparison between the two indexes will allow for a validation of  $IC$ .

$$FIC = \frac{Su + Sd}{2}$$

$FIC$  is subdivided into an upslope ( $Su$ ) and a downslope subfactor ( $Sd$ );  $FIC$  varies between 1 and 100 and increases with connectivity

$$Su = Au + Bu + W_u Cu_1 + (1 - W_u) Cu_2$$

Upslope subfactor

$$Sd = Ad + Bd + Cd + W_{d1} Dd_1 + (1 - W_d) Dd_2$$

Downslope subfactor

**Au** and **Ad**- Upslope area and the downslope distance to local sink;

**Bu** and **Bd** - Presence of sedimentation features along the upslope and downslope flow paths;

**Cd** presence and wideness of buffer-bush strip area before or along the flow path to the local sink;

**Cu1**, **Cu2**, **Dd1**, **Dd2** - Subfactors opposing resistance to fluxes (surface roughness and vegetation cover crop, plant basal area) in the upslope area and the downslope flow path;

**Wu** and **Wd** – Fraction of arable land in the upslope area and in downslope flow path.

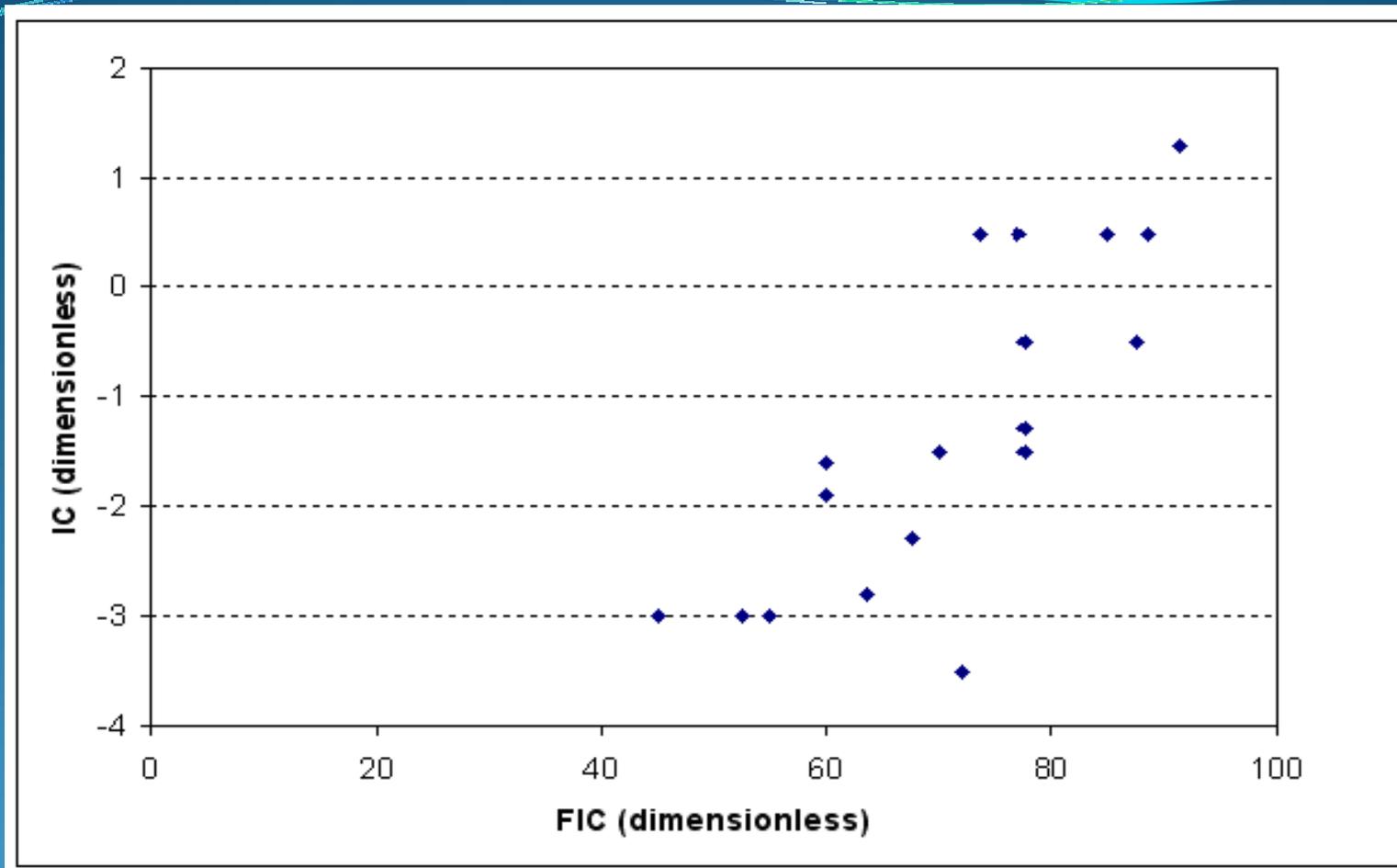
## Application at watershed scale (Bilancino Tuscany Italy, 150 km<sup>2</sup>)

To evaluate the degree to which the map represented real sediment flow connectivity, we compared it with field observations, conducted in autumn–winter 2003-2004 after several rainfall events of medium magnitude for the area.

During the surveys, 18 hot spot areas were identified within the watershed in proximity of the main streams. They are representative of the landuse and management of the basin

	SOIL USDA classification (8 <sup>th</sup> ed.1998)	LAND USE	Rainfall	Season	
Site1	Typic Udorthents fine mixed mesic	Wheat crop at the beginning of the growing season	2 events 30 mm/day	Autumn	
Site 2	Typic Udorthents clayey skeletal, mixed mesic	Wheat crop at the beginning of the growing season	2 events 30 mm/day	Autumn	
<i>Sub Factors</i>	<i>Component</i>	<b>Site 1a</b>	<b>Site 1b</b>	<b>Site 2a</b>	<b>Site 2b</b>
<b>Au</b>	UPSLOPE COMPONENT	45	45	45	30
<b>Bu</b>		20	5	20	5
<b>Cu1</b>		5	5	10	10
<b>Cu2</b>		-	-	20	-
<b>Wu</b>		1	1	0.8	1
<b>Ad</b>	DOWNSLOPE COMPONENT	40	40	20	20
<b>Bd</b>		20	10	15	10
<b>Cd</b>		20	20	20	10
<b>Dd1</b>		-	-	-	-
<b>Dd2</b>		20	10	15	5
<b>Wd</b>		1	1	1	1
<b>Connectivity indexes</b>					
<b>FIC</b> (eq. 10)		85	67.5	85	45
<b>IC</b> (eq. 7)		0.5	-2.3	0.5	-3

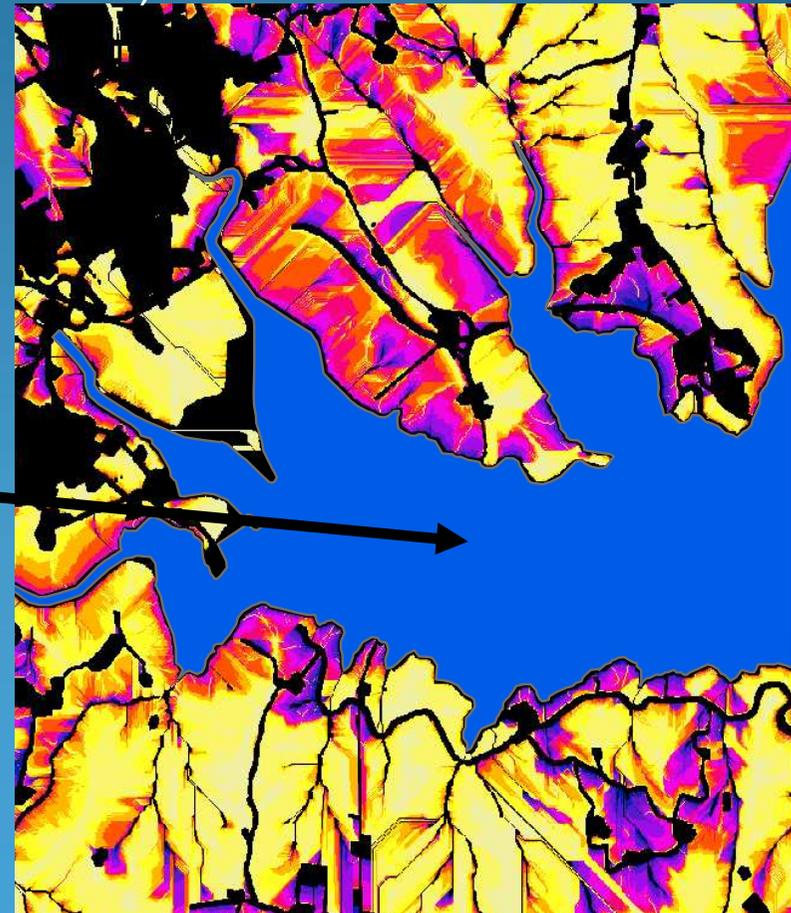
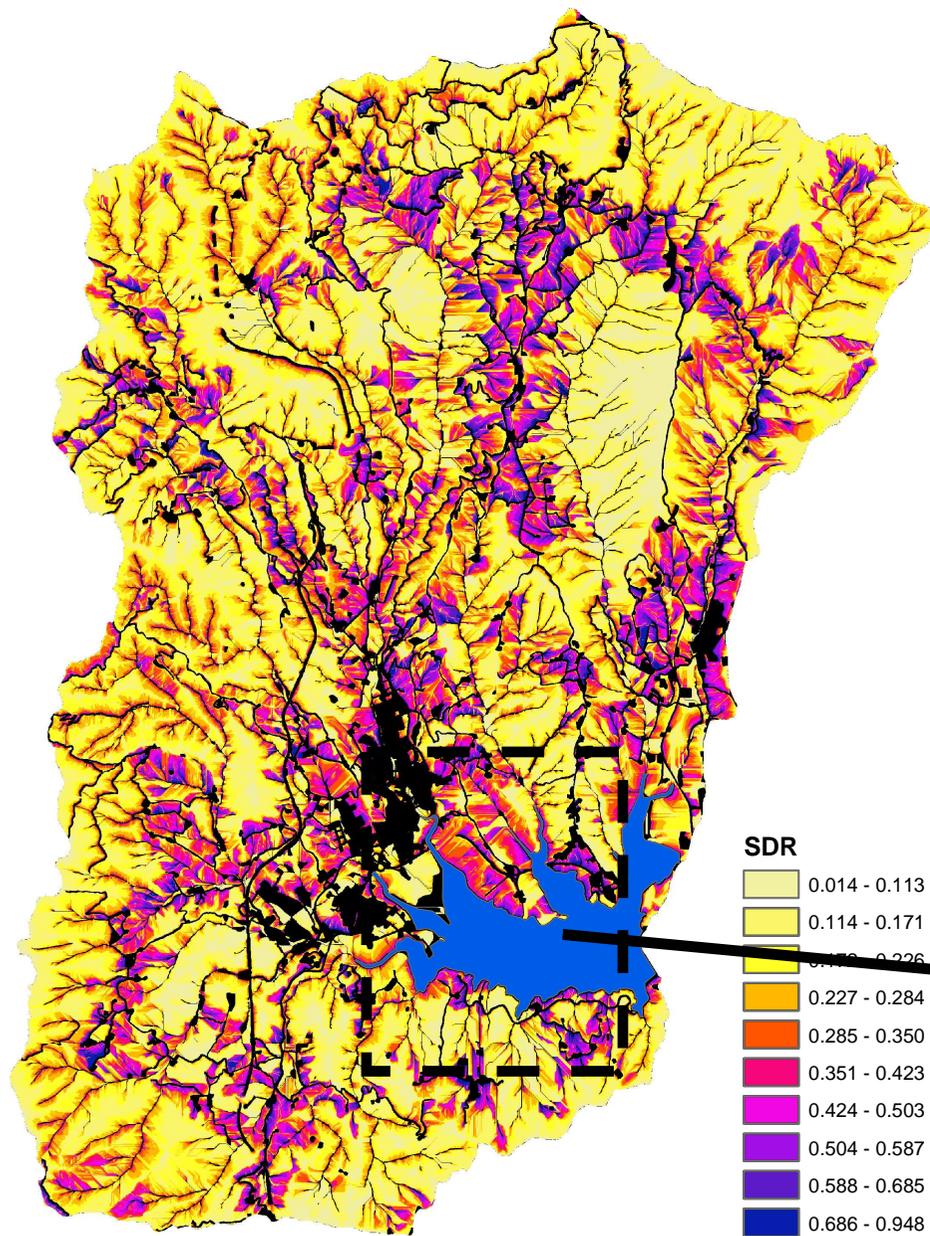
Subfactors for field assessment of connectivity index *FIC*. The last row reports and the corresponding values of *IC*

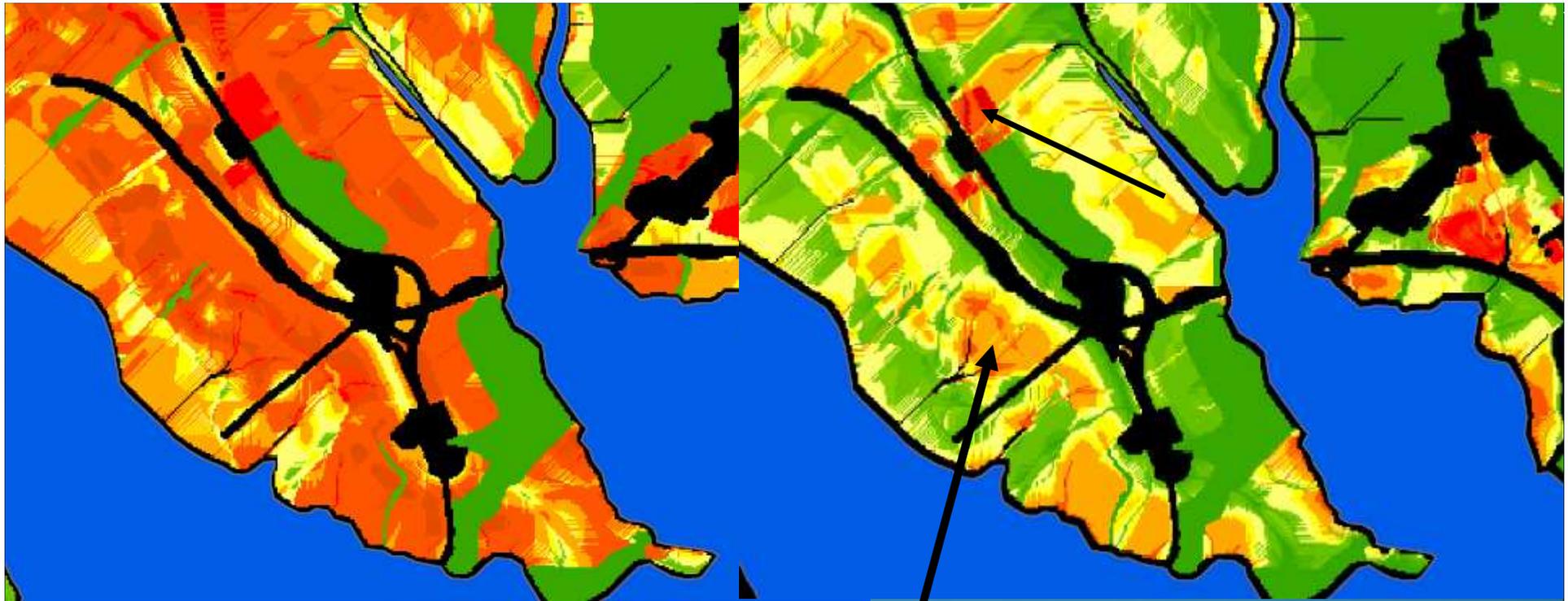


The FIC values have been compared to the IC flux map obtained with the ArcGIS procedure for the entire study site

## SDR maps distribution in an entire watershed for average annual erosion rate correction

Many authors have used the SDR to correct the distributed soil erosion model's output (Ferro and Porto 2000; Lu et al., 2006)





**Local Average erosion rate...  
Classic RUSLE3D**

**Average sediment yield  
Contribution:  
RUSLE3D corrected  
according to  $I_c$  and SDR**

# SDRmax

**SDRmax is the maximum SDR can occur in a given place and in a given interval of time.**

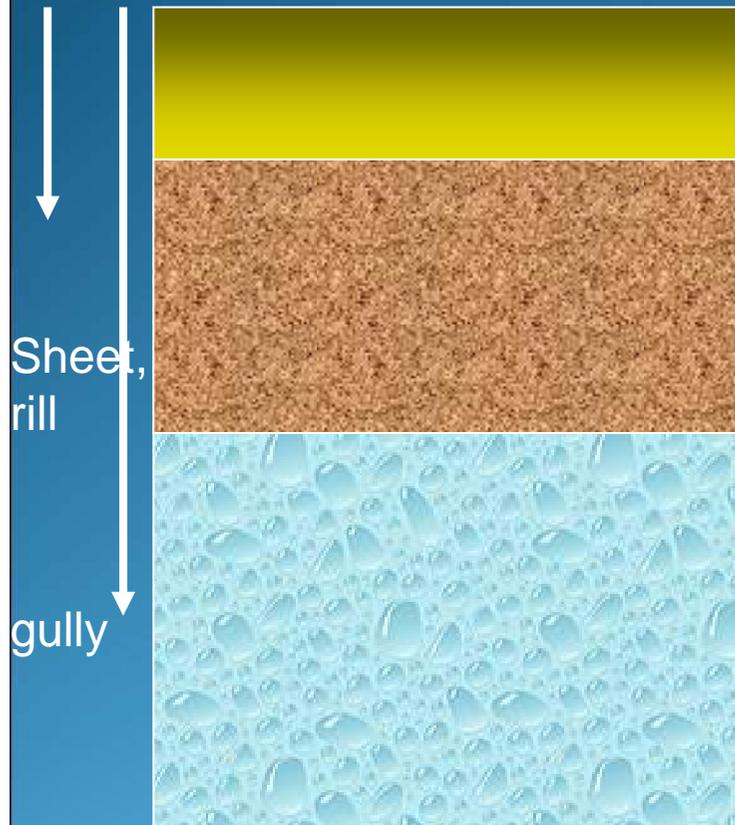
**For geological time the SDR is 1.0 everywhere!**

**For much shorter interval of time it may be lower...**

**DT= 1day, 1 year, 10 year... (it depend form distance and travel speed... Or in other words from the dominant erosion processes**

**It should depends on different mobility of the textural class of sediments (clay, loam , sand, gravel, boulder) that are in soil profile.. (Lu 2003, 2006)**

**SDRmax may be obtained by weighed average of each SDRmax of the different horizons that can be mobilised by the considered soil erosion processes (e.g. Gully , rill; sheet ..)**



30% C; 40% L; 20% S; 10% R → SDRmax=0.8

10% C; 30% L; 40% S; 20% R → SDRmax=0.5

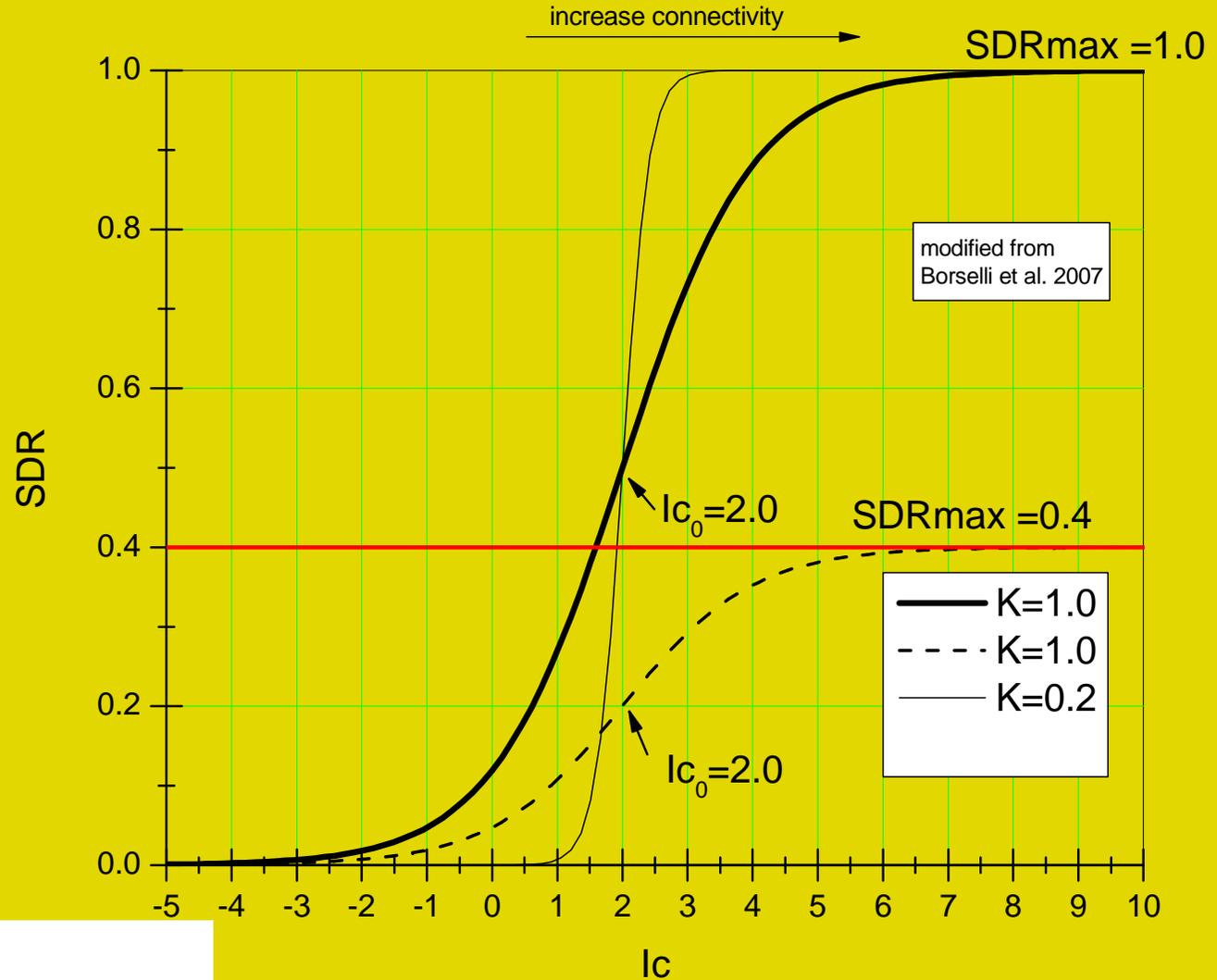
0% C; 5% L; 25% S; 80% R → SDRmax=0.2

Global SDRmax in this case  
Is about 0.5 (gully ?)

**SDRmax for each text.class can be obtained using the Lu (2003,2006) algorithm knowing soil profile data and the defined  $\Delta T$  .**

# Generalised functional relationships between $I_c$ and SDR...

## The definition of SDRmax



$$SDR = \frac{SDR_{Max}}{1 + \exp\left(\frac{I_{c_0} - I_c}{k}\right)}$$

## Others Possible integrations between soil erosion and connectivity assessment models:

- Flow connectivity approach (FCA) is easy to apply to large catchments
- **FCA can identify problematic areas**
- Models can then be applied only to these spots (saving time and money) and be used for designing conservation strategies (CS)

## And More... Application of connectivity TO LANDSLIDES (work in progress...)



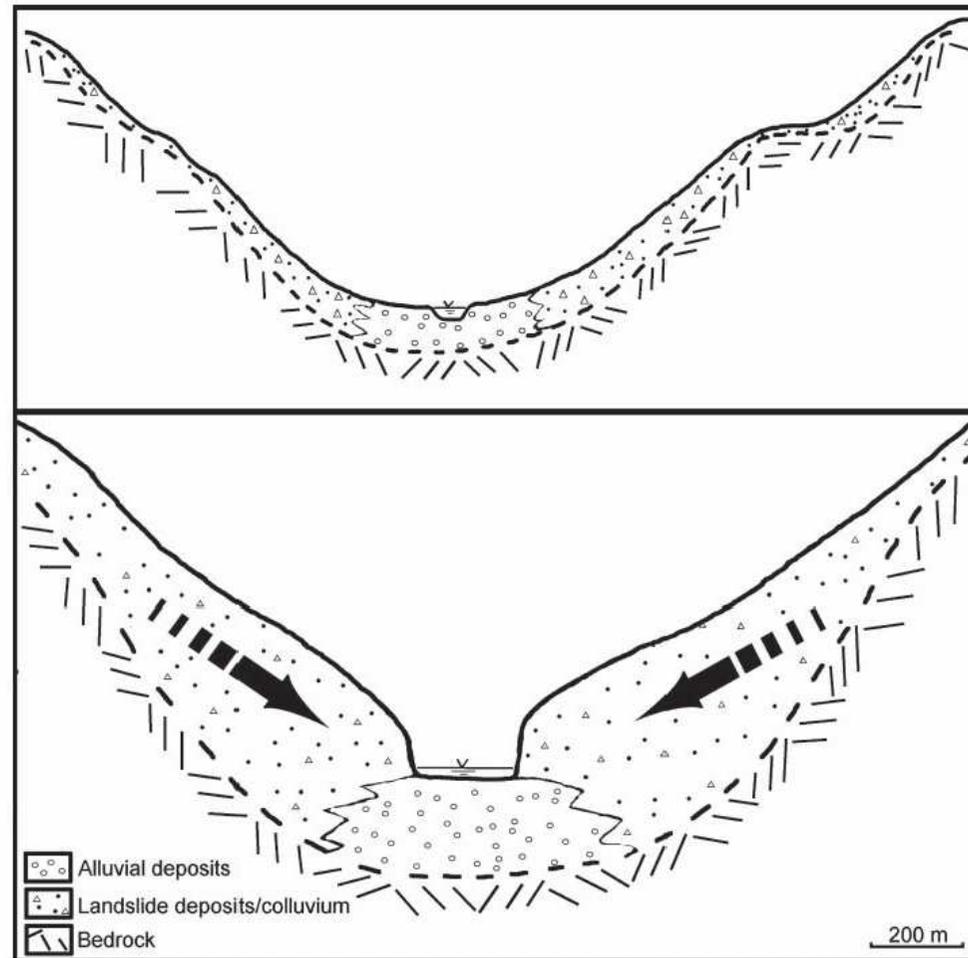
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Samoggia Valley  
(north Italy)

**2 October 2002  
(200 mm rainfall  
in september)**



## APPLICATION TO LANDSLIDES: landslides contribution to sediment yield



**Figure 10.** Typical cross-sections of two contrasting valleys. *Top:* valley with no dominant landslides. *Bottom:* valley with abundant landslides that supply lots of sediment to the ephemeral channel.

## DIFFUSE SURFACE LANDSLIDE IN A BADLAND AREA



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## ...LANDSLIDE DISTRIBUTION, DEPTH AND VOLUMES.

Application a distributed slope stability model  
Es. Sinmap, Shalstab or an alternative model  
like *montecarlo methods* applied to entire  
watershed

## Limit equilibrium - Infinite slope model

Potential sliding mass

$$F_s = \frac{\left( \frac{c'}{\gamma z} + (\cos^2 \beta - r_u) \tan \phi' \right)}{\sin \beta \cos \beta}$$

where:

$\beta$  = slope gradient (degrees)

$\phi'$  = internal friction angle (degrees)

$c'$  = soil cohesion + roots strength (kPa)

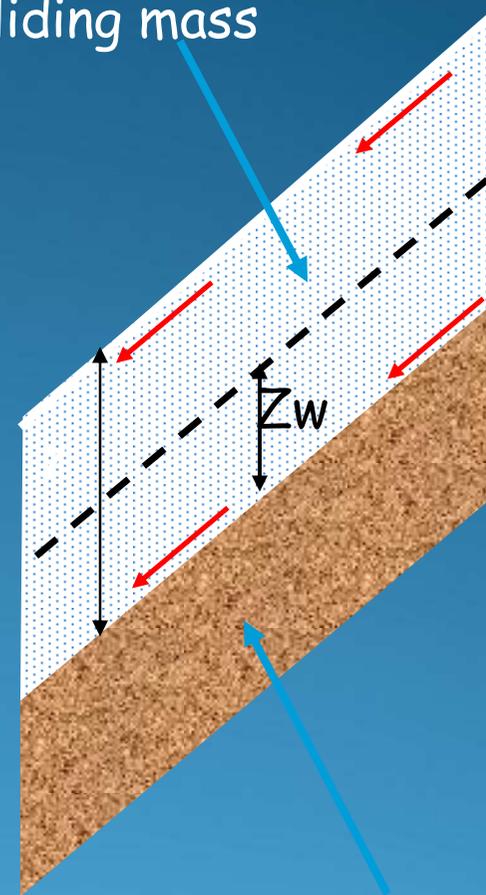
$\gamma$  = soil unit weight (kN/m<sup>3</sup>)

$Z$  = depth of sliding surface (in m)

$Z_w$  = depth of water saturated horizon

$r_u$  = coefficient of interstitial pressure (adimensional)

$$r_u = \frac{9.81 * z_w}{\gamma}$$



Bedrock stable mass

**If  $F_s < 1.0$  = unstable condition**

# Limit equilibrium - Infinite slope model

## Fields of application

- Planar uniform slope
- Debris/soil over stable bedrock
- Translational landslides (failure surface parallel to slope)
- Possibility of application in GIS systems (e.g. SHALSTAB, SINMAP)
- Trigger conditions for debris flow and mud slide (Iverson, 2000)

## Advantages

- Easy to implement in spreadsheets and programs
- Easy and fast computation

## Disadvantages

- Static approach (e.g. fixed depth of saturated horizon)
- It Need to iterate the computation for several conditions: (infiltration/rainfall,  $Z$ ,  $Z_w$ ..), soil properties variability and local gradient  $\beta$  of the slope

# Limit equilibrium method, Infinite slope model, and Monte Carlo Method

Local variability of soil properties  
Local variability of slopes  
Groundwater depth

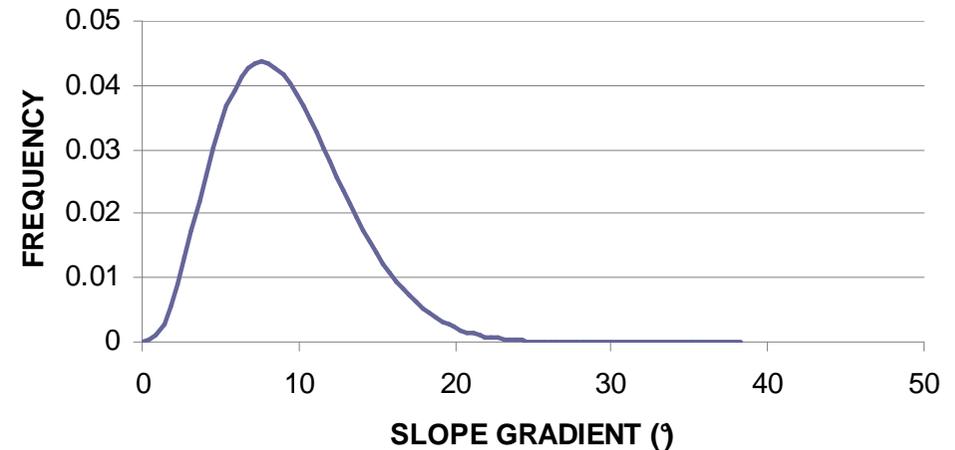
Random variables  
e.g. uniformly distributed  
Between lower and upper bounds:  
 $10^\circ < \phi' < 14^\circ$   
 $2 < c' < 5$

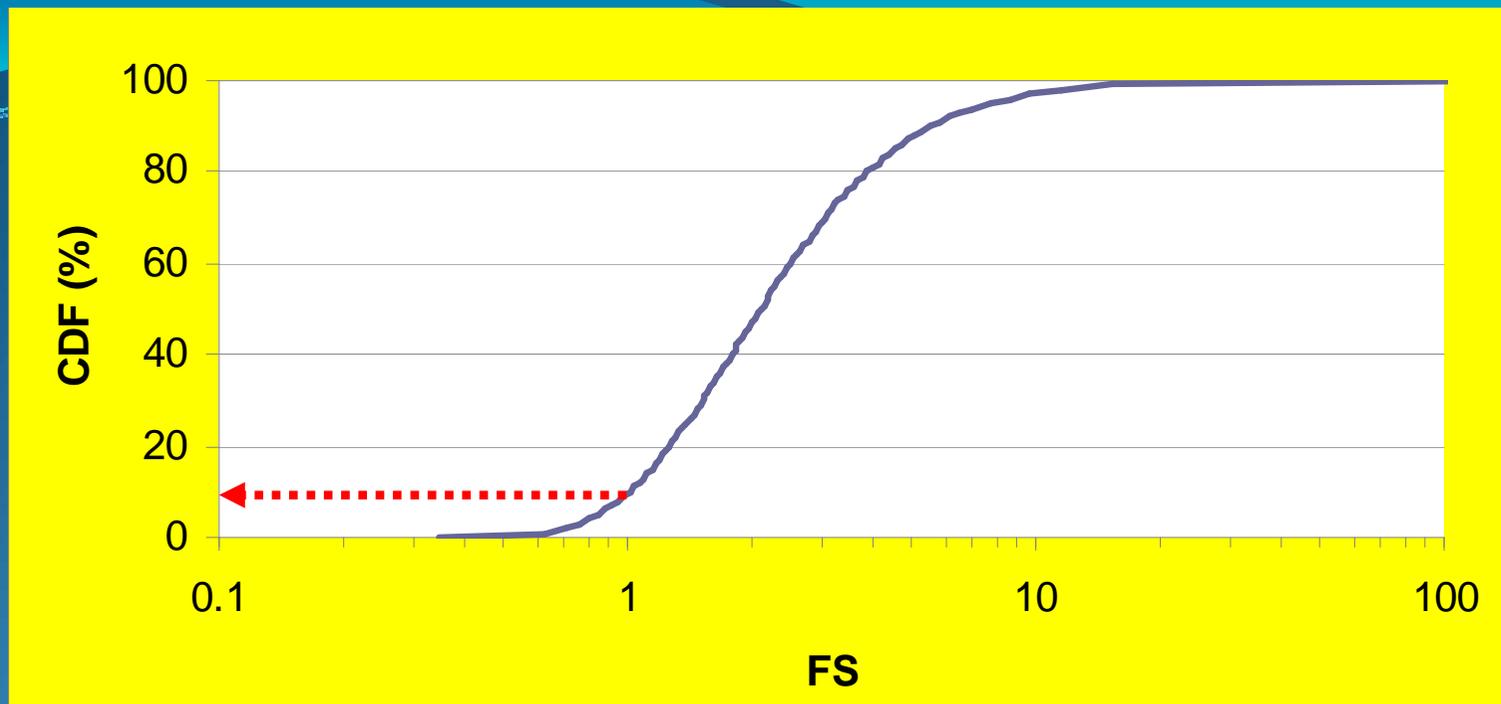
<u>alpha</u>	2.64	0	grad min
<u>beta</u>	10.43	0.79	grad max

	c' (kPa)	$\phi'$ (°)	ru	$\beta$ (°)	$\gamma$ (kNm <sup>3</sup> )	z(m)
min	2	10	0.5	0	17	0.5
max	5	14	0.5	38.3087	19	1.5

The safety factor  $F_s$   
Is a random variable  
It accounts for local  
Variability of the input  
Parameters...

SLOPE SPECTRUM



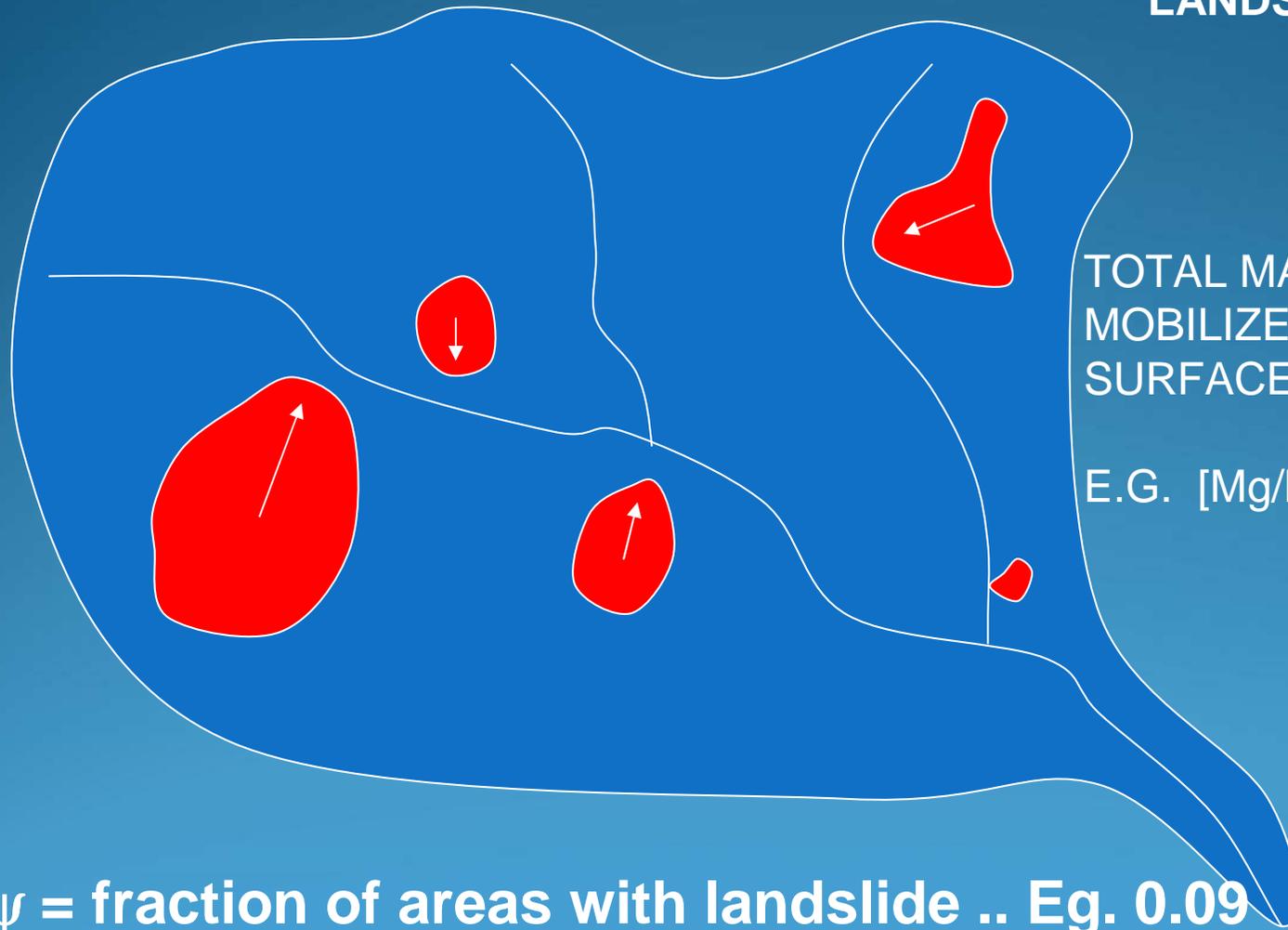


**9% of entire watershed has  $FS < 1.0$**

**Using the slope spectrum of a entire watershed the % of  $FS < 1.0$  represents the potential fraction of total area affected by landSlides ( $\Psi$ )**

# Total LANDSLIDE VOLUME from area and average depth of landslides

IT APPLIES AT SHALLOW LANDSLIDE ONLY..



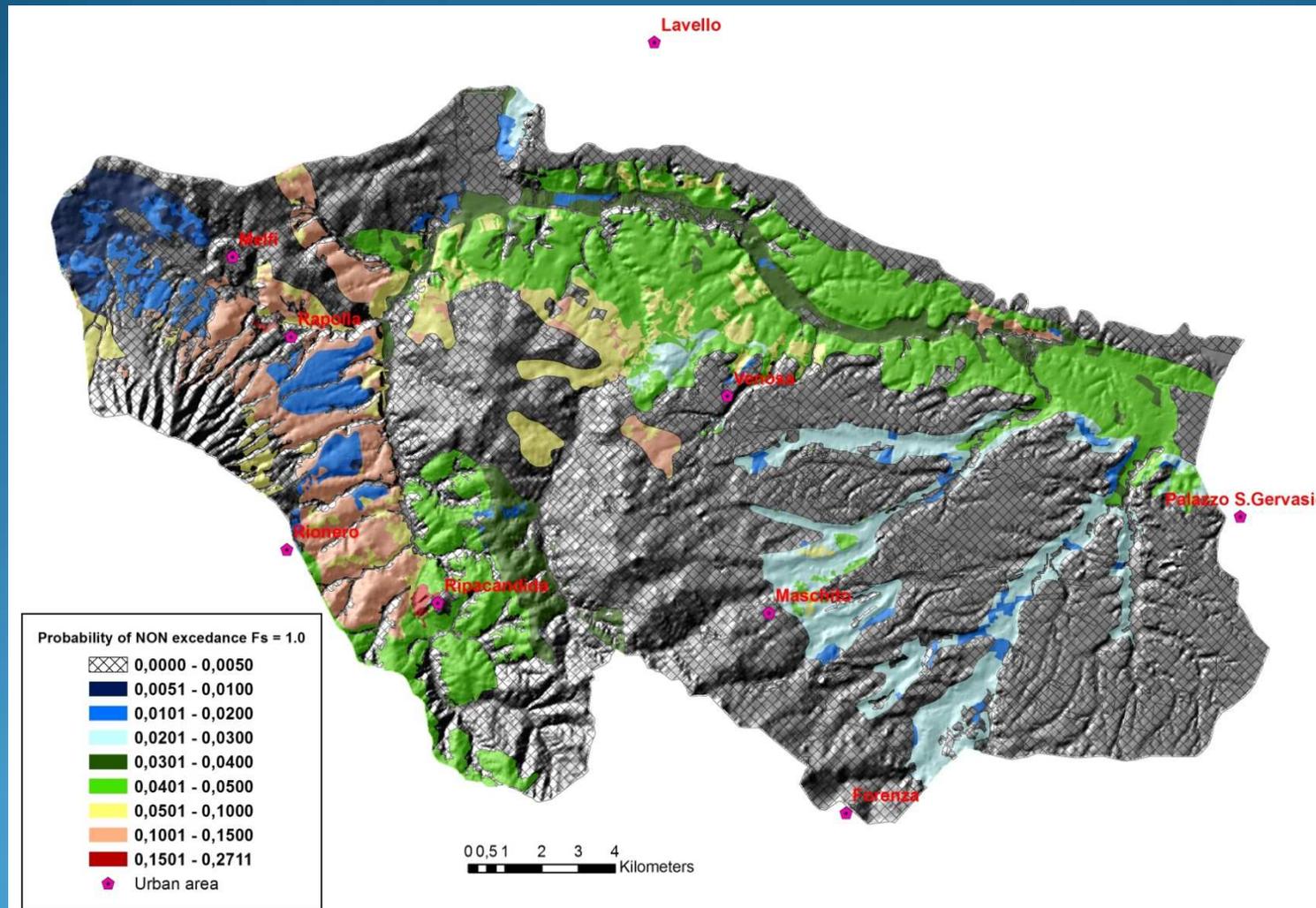
TOTAL MASS THAT CAN BE MOBILIZED FOR SPECIFIC SURFACE IN A WATERSHED

E.G. [Mg/km<sup>2</sup>]

$\psi$  = fraction of areas with landslide .. Eg. 0.09

# Shallow landslides extension to PESERA

It is One of the CNR-IRPI Activities within  
DESIRE project – Rendina Dam catchment (south, italy)



## ...Sediment delivery ratio for landslides:SDRL

The same definition of previous SDR can be applied also to shallow landslides contribution because only a fraction of landslide volume can contribute to sediment yield...

USUALLY SDRL SHOULD BE LOWER THAN SDR... BUT IN EXTREME CONDITION IT IS VERY HIGH (SDRL > 0.5)

case studied

Sestino (Tuscany- Marche border)

Parent material : clay shales and olistostromes (Eocene)  
(structurally complex formations)



Altitude  
1000- 1100 m

Mean annual  
Precipitation  
(snow included)  
1200 mm

Several  
snowmelting  
events during the  
winter !!



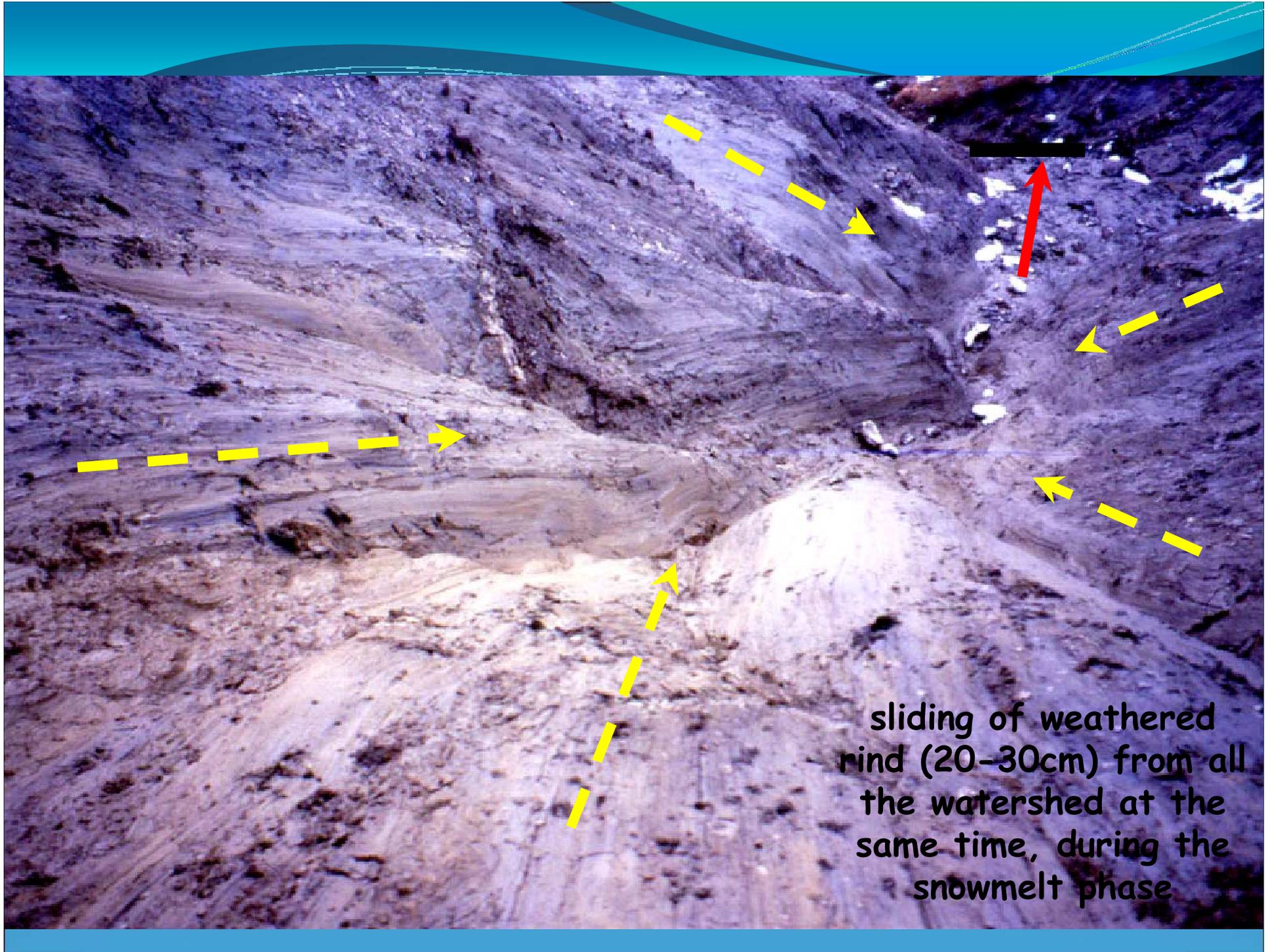
Badland area where the main Erosion process is shallow landsliding

Translational landslides of weathered rind formed from clay shales parent material

Temporary accumulation at the valley bottom and subsequent mudflow

(computed average depth erosion rate:  
0.2-0.05 m/y)





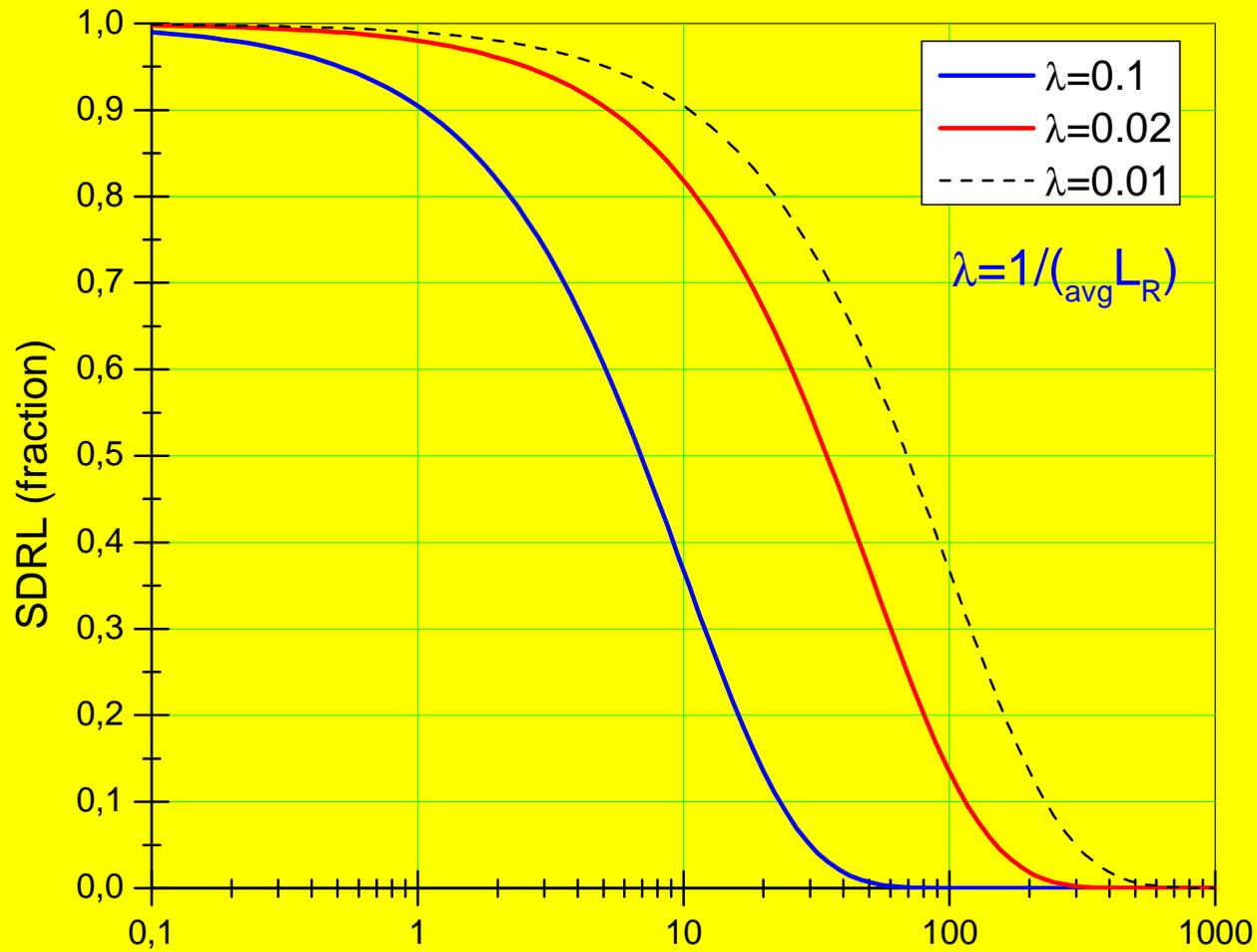
sliding of weathered rind (20-30cm) from all the watershed at the same time, during the snowmelt phase

# Mudflow – gully runout distance



# probabilistic model of landslides and debris flow delivery to stream channels

( Miller & Burnett, 2008)

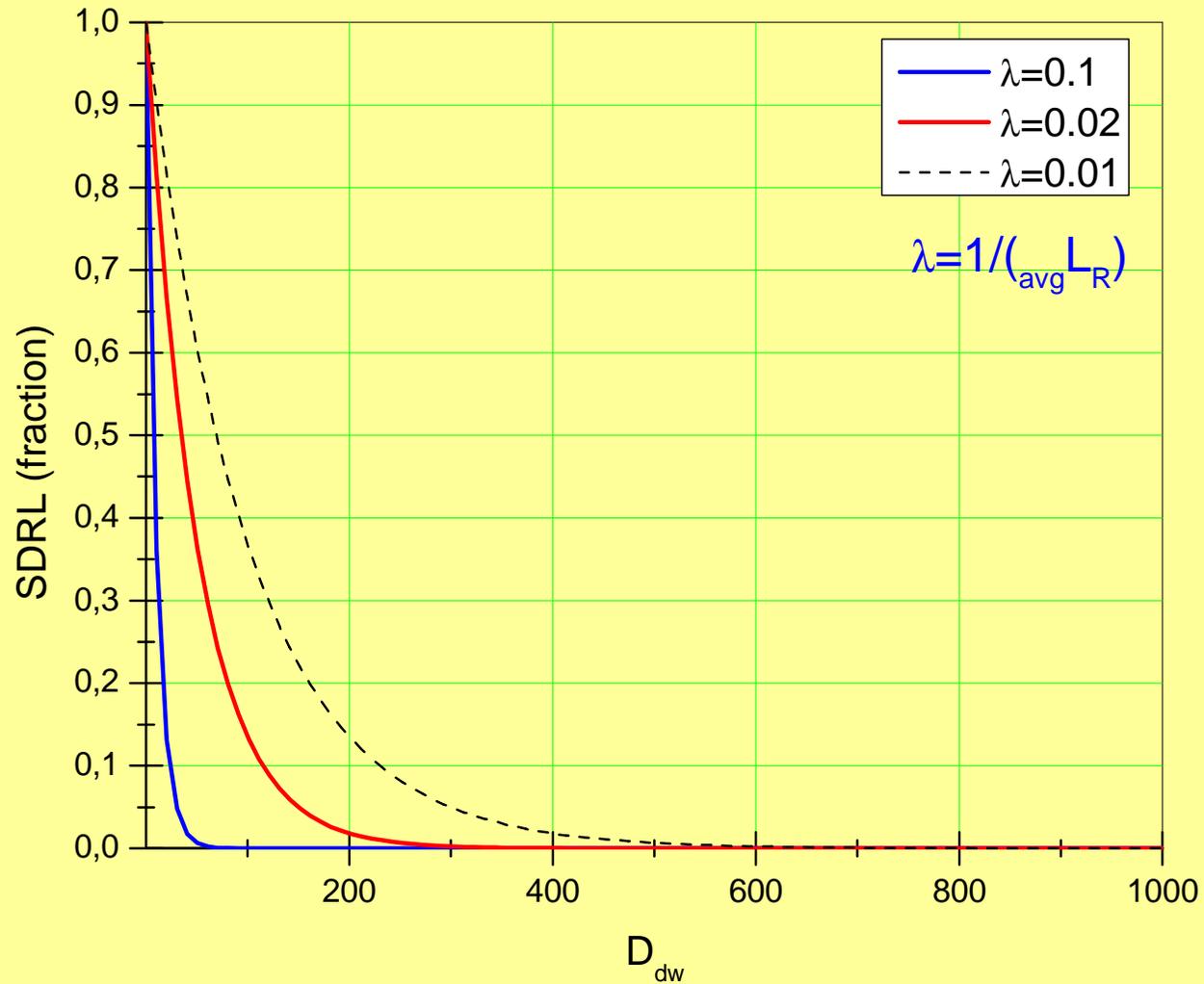


$D_{dw}$

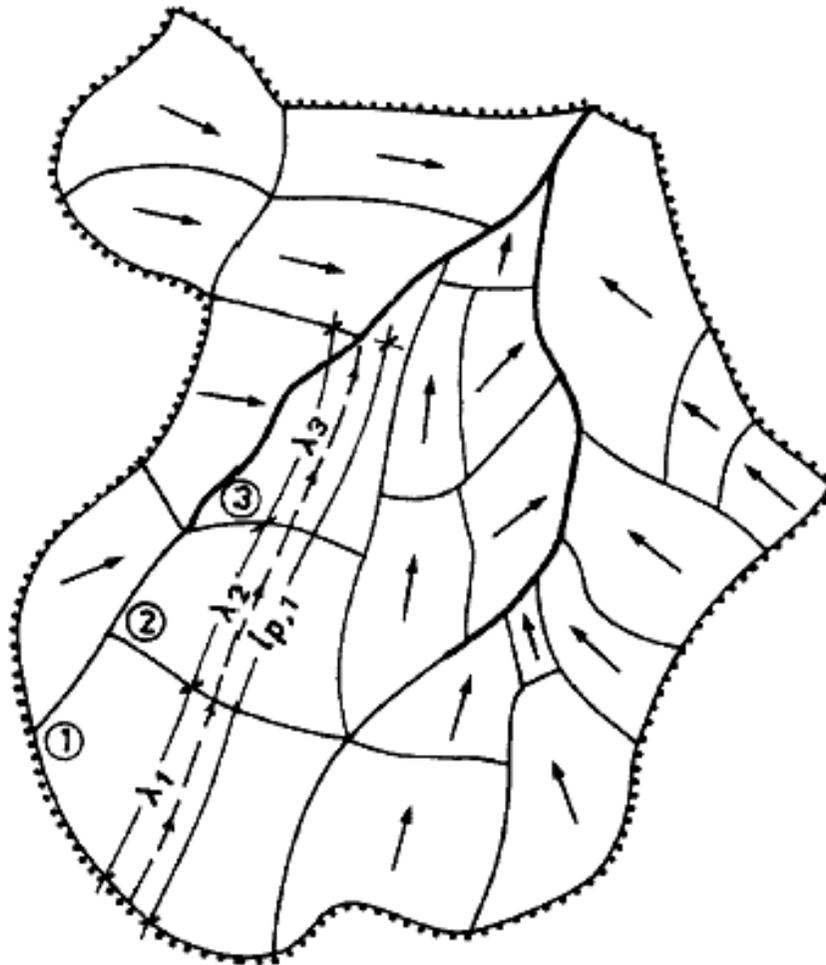
Downsloper component of IC index

## probabilistic model of landslides and debris flow delivery to stream channels

( Miller & Burnett, 2008)



**Exponential probability distribution function**  
**Depends from the average runout length  $L_r$  (measured)**  
**and the local site  $D_{dw}$  distance to a sink**



- basin boundary
- stream
- morphological unit boundary
- main flow direction

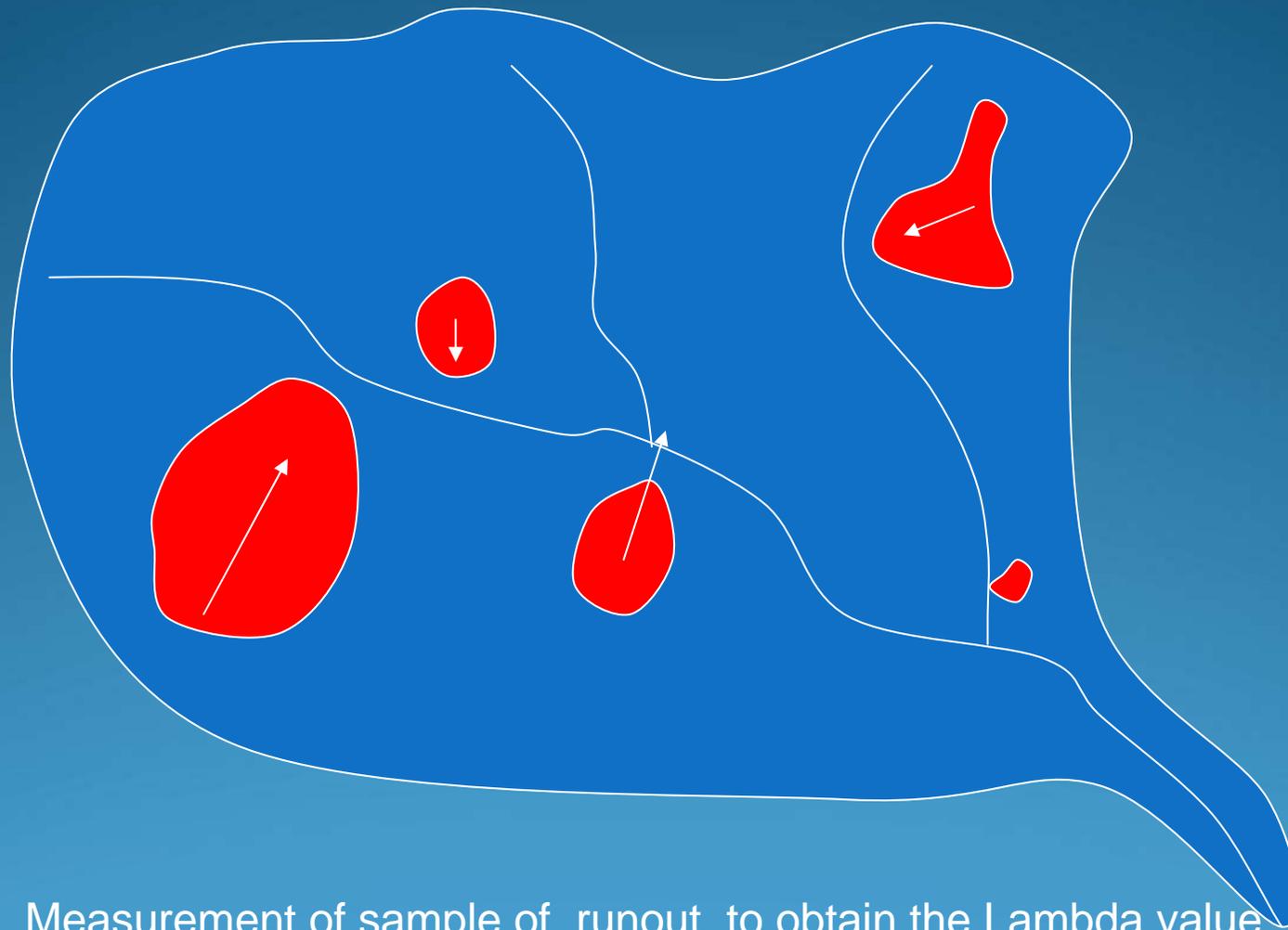
FIG. 1. Scheme of Basin Discretized into Morphological U

## Ferro & Porto 2000 (SEDD model)

$$SDR_j = \exp \left[ -\beta \left( \sum_{j=1}^n \frac{\lambda_j}{\sqrt{s_j}} \right) \right]$$

$\beta$  = lumped calibration parameter  
 $\lambda$  = length along flow path  
 $s$  = slope along flow path

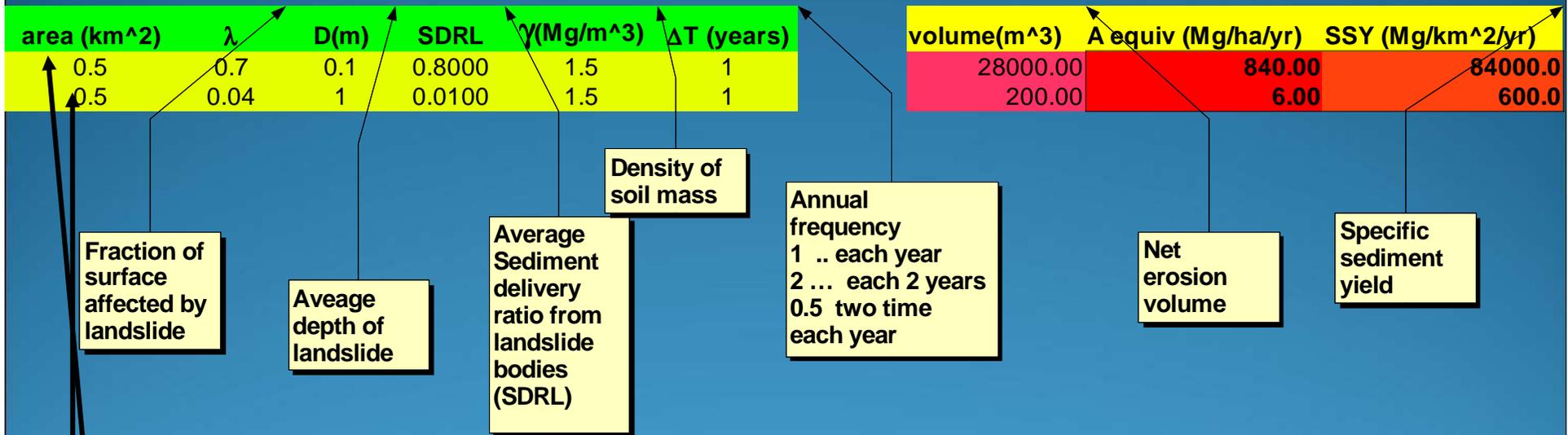
In this case SDR it is computed and applied at each morphological units to obtain the single sediment yield contribution



Measurement of sample of runout to obtain the Lambda value

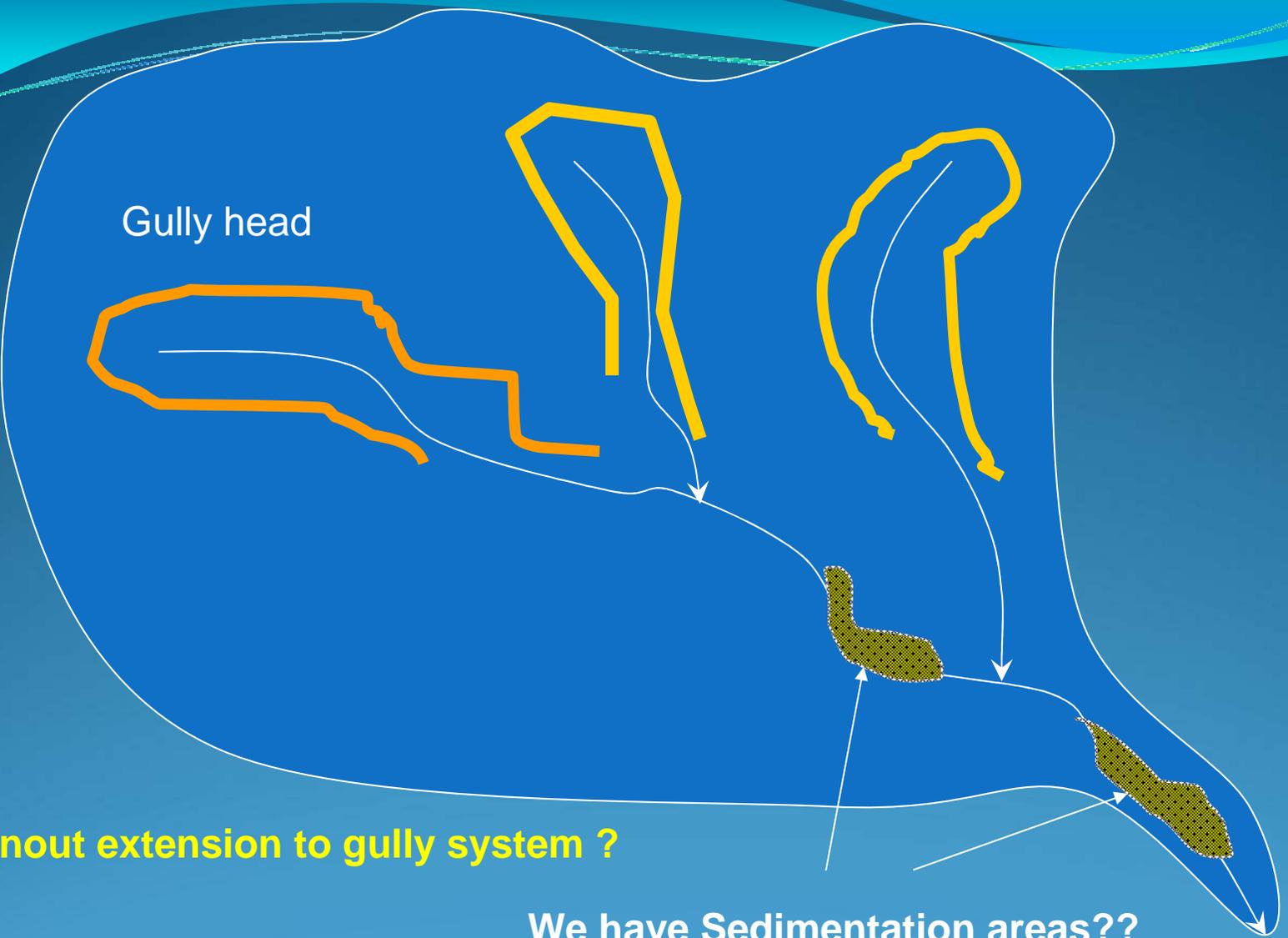
# Specific Sediment yield due to landslide only

## Two examples of computation



The first row represents the situation of Sestino site **840 Mg/km<sup>2</sup>/yr**

The second row represent an area affected of relevant fraction of shallow landslides less connected to drainage system **6 Mg/km<sup>2</sup>/yr**



The diagram shows a gully system on a blue background. A large area on the left is labeled 'Gully head'. Three yellow-outlined paths originate from this area and flow towards the right. These paths converge into a single path that leads to two green, textured areas representing sedimentation zones. White arrows indicate the direction of flow from the gully head through the paths to the sedimentation areas.

Gully head

**Runout extension to gully system ?**

**We have Sedimentation areas??**

Integration processes for multi source.. ?

## Conclusions

The Connectivity index and FCA **provides an estimate of the potential connection index between the sediment eroded from hillslopes and the stream system;**

FCA can put in relation the IC index and SDR. SDR can be used then to correct the USLE-TYPE models (*transport capacity unlimited*) generally used for large catchments modelling end obtain a Sediment yield assessment

The use of SDRmax can correct the inconsistencies indicated by someone  
(Kinnell 2004, Parson et a. 2006)

## Conclusions-2

The IC model have a large set of potential applications such as **hot spot identification of primary sediment sources** to permanent drainage lines and **verification of effects of eco-compatible mitigation measures to reduce or increase connectivity** . (without more complex Soil erosion models) (e.g. indications of Boardman 2006)

Potential application of IC to define **SDRL** can help to assessment of Sediment yield contribution due to Landslides (*work in progress..*) and gullies may be..



**Many  
Thanks for your  
attention ...**